
RF Pulse Design: RF Pulses, Adiabatic Pulses

M229 Advanced Topics in MRI

Holden H. Wu, Ph.D.

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UCLA

*Department of Radiological Sciences
David Geffen School of Medicine at UCLA*

Class Business

- Office hours
 - Holden: by appointment
 - Wenqi (HW1): 10-12 on 4/18 Fri
 - Timo (HW2): 4/18, 4/24, 4/25
 - Email beforehand
- Homework 1 due on 4/21 Mon
- Homework 2 due on 4/28 Mon
- Final project
 - Start thinking

Outline

- Review of RF pulses
- Adiabatic passage principle
- Adiabatic inversion
- Applications of adiabatic pulses
- MATLAB demo

Review of RF Pulses

RF Pulses

- What do RF pulses do?
- Challenges at higher B_0 fields?

Notation and Conventions

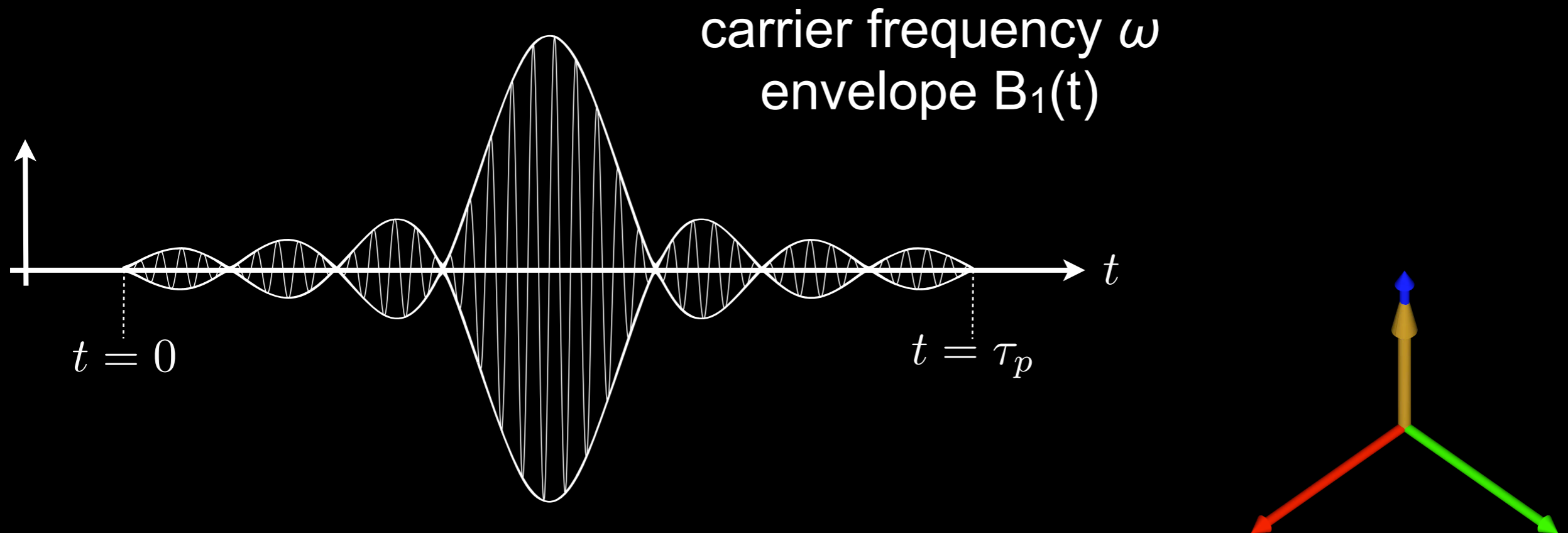
$$\vec{B} = B_0 \hat{k} + B_1(t) [\cos \omega t \hat{i} - \sin \omega t \hat{j}]$$

- ω = carrier frequency
- ω_0 = resonant frequency
- $B_1(t)$ = complex valued envelope function

RF Pulse - Excitation

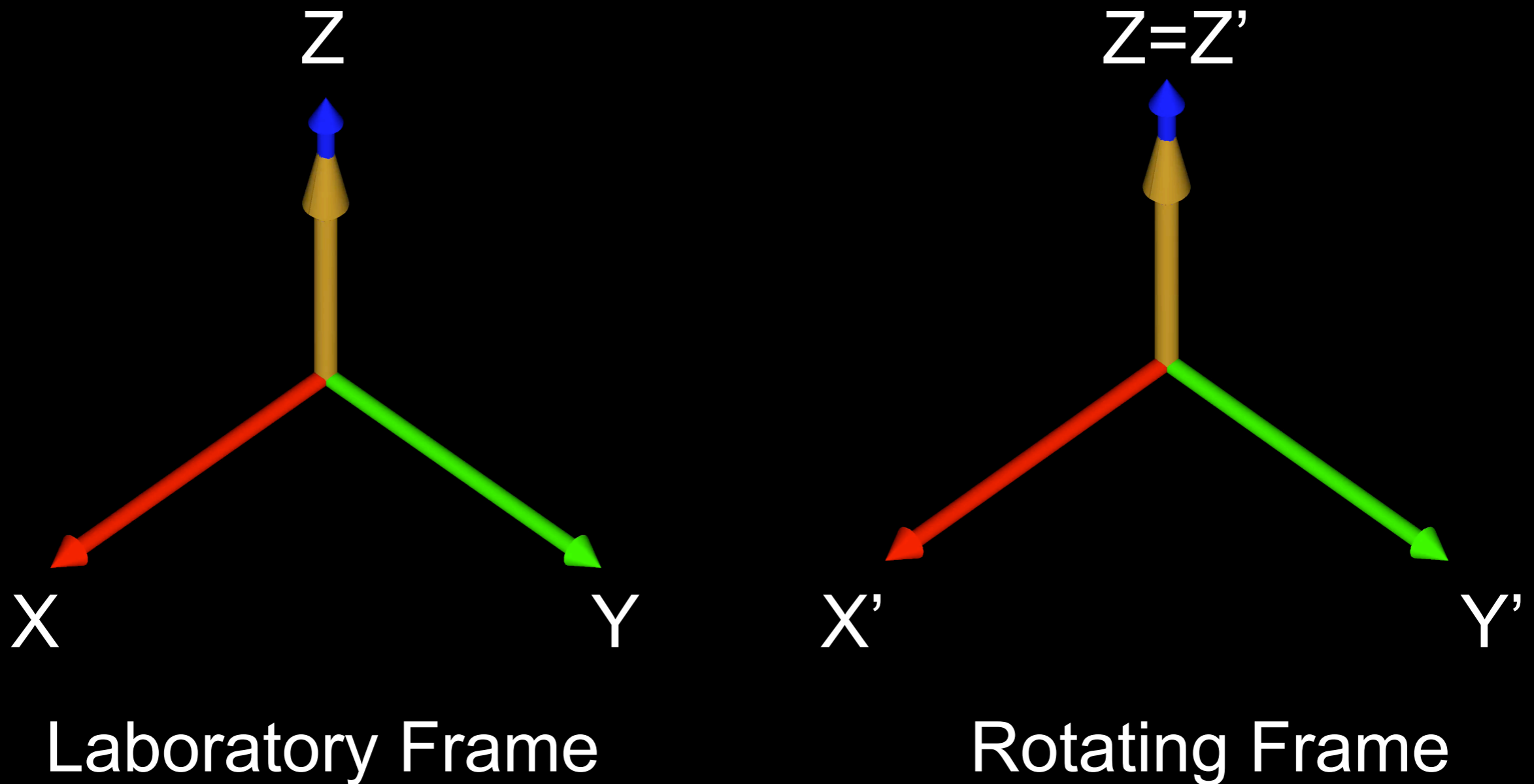
$$\vec{B} = B_0 \hat{k} + B_1(t) [\cos \omega t \hat{i} - \sin \omega t \hat{j}]$$

$$B_1(t) \cdot [\cos(\omega t) \hat{i} - \sin(\omega t) \hat{j}]$$



Lab vs. Rotating Frame

- The rotating frame simplifies the mathematics and permits more intuitive understanding.



Rotating Frame

Rotating Frame Definitions

$$\vec{M}_{rot} \equiv \begin{bmatrix} M_{x'} \\ M_{y'} \\ M_{z'} \end{bmatrix} \quad \vec{B}_{rot} \equiv \begin{bmatrix} B_{x'} \\ B_{y'} \\ B_{z'} \end{bmatrix} \quad \begin{array}{l} B_{z'} \equiv B_z \\ M_{z'} \equiv M_z \end{array}$$

$$\vec{M}_{lab}(t) = R_Z(\omega_0 t) \cdot \vec{M}_{rot}(t)$$

$$\vec{B}_{lab}(t) = R_Z(\omega_0 t) \cdot \vec{B}_{rot}(t)$$

$$\frac{d\vec{M}}{dt} = \vec{M} \times \gamma \vec{B} \quad \longrightarrow \quad \frac{d\vec{M}_{rot}}{dt} = \vec{M}_{rot} \times \gamma \vec{B}_{eff}$$

Bloch Equation (Rotating Frame)

$$\frac{d\vec{M}_{rot}}{dt} = \vec{M}_{rot} \times \gamma \vec{B}_{eff}$$

where $\vec{B}_{eff} = \vec{B}_{rot} + \frac{\vec{\omega}_{rot}}{\gamma}$ fictitious field

$$\vec{\omega}_{rot} = \begin{pmatrix} 0 \\ 0 \\ -\omega \end{pmatrix}$$

Bloch Equation (Rotating Frame)

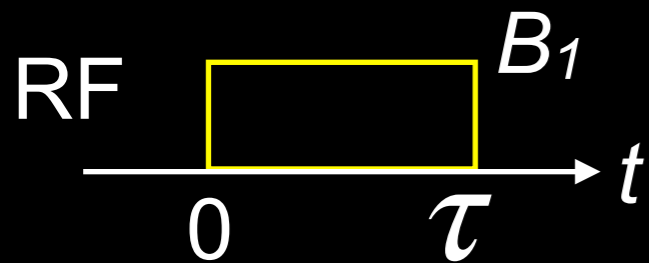
$$\vec{B}_{eff} = \vec{B}_{rot} + \frac{\vec{\omega}_{rot}}{\gamma}$$

$$\vec{B}_{lab} = \begin{pmatrix} B_1(t) \cos \omega_0 t \\ B_1(t) \sin \omega_0 t \\ B_0 \end{pmatrix} \quad \vec{B}_{rot} = \begin{pmatrix} B_1(t) \\ B_1(t) \\ B_0 \end{pmatrix}$$

Assume real-valued $B_1(t)$

$$\vec{B}_{rot} = \begin{pmatrix} B_1(t) \\ 0 \\ B_0 \end{pmatrix} \quad \vec{B}_{eff} = \begin{pmatrix} B_1(t) \\ 0 \\ B_0 - \frac{\omega}{\gamma} \end{pmatrix}$$

Bloch Equation (Rotating Frame)



$$B_1(t) = B_1; 0 \leq t \leq \tau$$

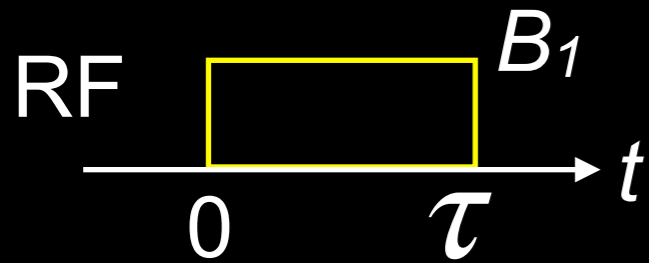
$$\vec{B}_{eff} = \begin{pmatrix} B_1 \\ 0 \\ 0 \end{pmatrix}$$

On resonance: $B_0 - \frac{\omega_0}{\gamma} = 0$

$$\frac{d\vec{M}_{rot}}{dt} = \vec{M}_{rot} \times \gamma \vec{B}_{eff} \quad \theta = \int_0^{\tau} \gamma B_1(t') dt' = \gamma B_1 \tau$$

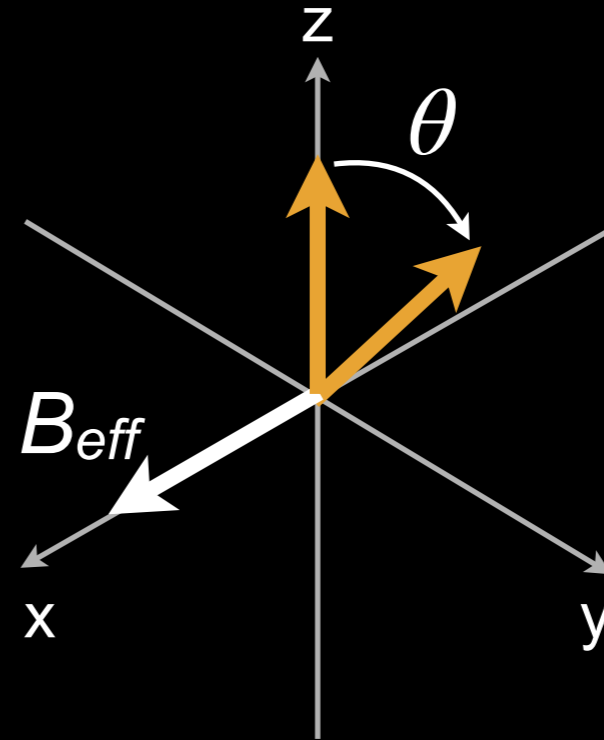
$$\Rightarrow \vec{M}_{rot}(t) = R_x(\theta = \gamma B_1 t) \begin{bmatrix} 0 \\ 0 \\ M_0 \end{bmatrix} = \begin{bmatrix} 0 \\ M_0 \sin(\theta) \\ M_0 \cos(\theta) \end{bmatrix}$$

Bloch Equation (Rotating Frame)



$$B_1(t) = B_1; 0 \leq t \leq \tau$$

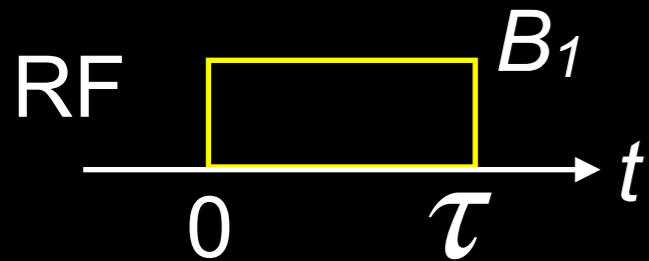
$$\vec{M}_{rot}(t) = \begin{bmatrix} 0 \\ M_0 \sin(\theta) \\ M_0 \cos(\theta) \end{bmatrix}$$



$$\theta = 90^\circ = \frac{\pi}{2}, \tau = 1ms$$

$$\frac{\pi}{2} = \gamma \cdot 1ms \cdot B_1 \quad \Rightarrow \quad B_1 \approx 0.66G = 6\mu T$$

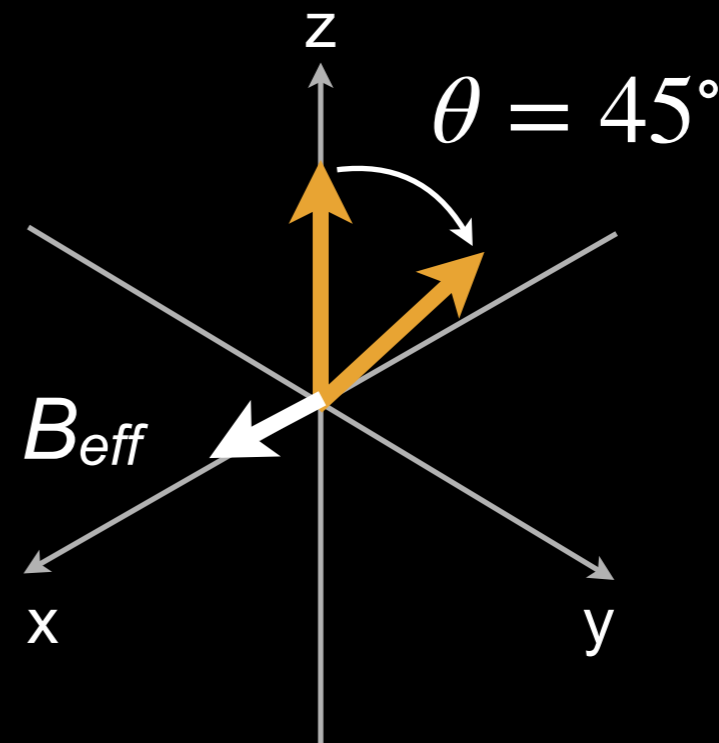
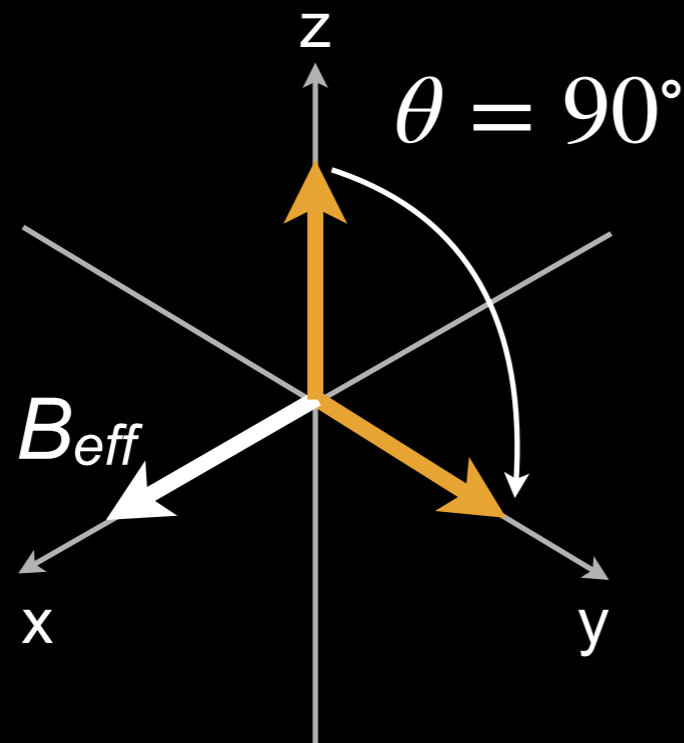
Bloch Equation (Rotating Frame)



$$B_1(t) = B_1; 0 \leq t \leq \tau$$

B_1 inhomogeneity:

B_1 reduced by 50%



Bloch Equation with Gradient

$$\frac{d\vec{M}_{rot}}{dt} = \vec{M}_{rot} \times \gamma \vec{B}_{eff}$$

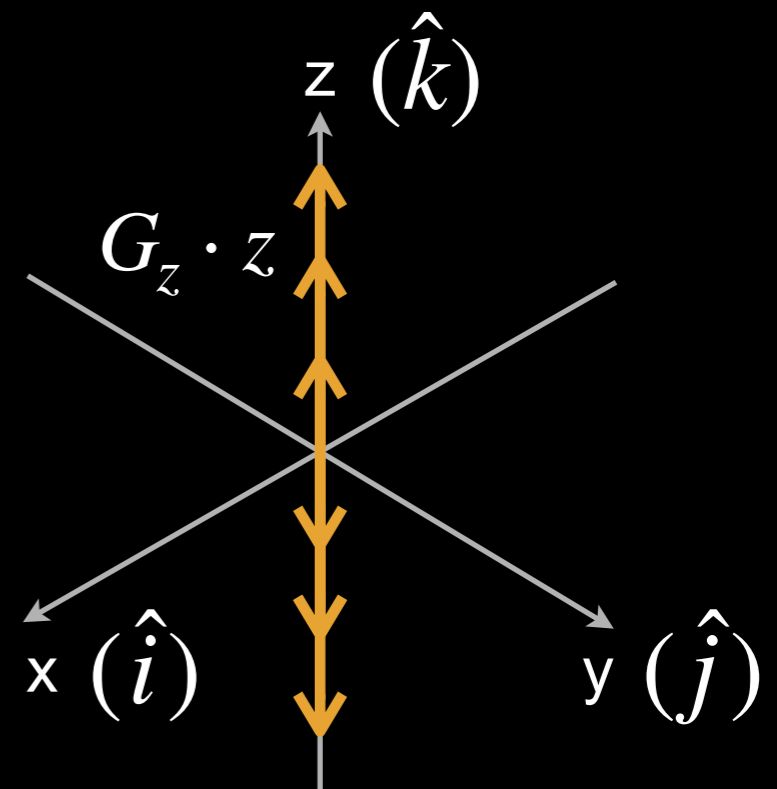
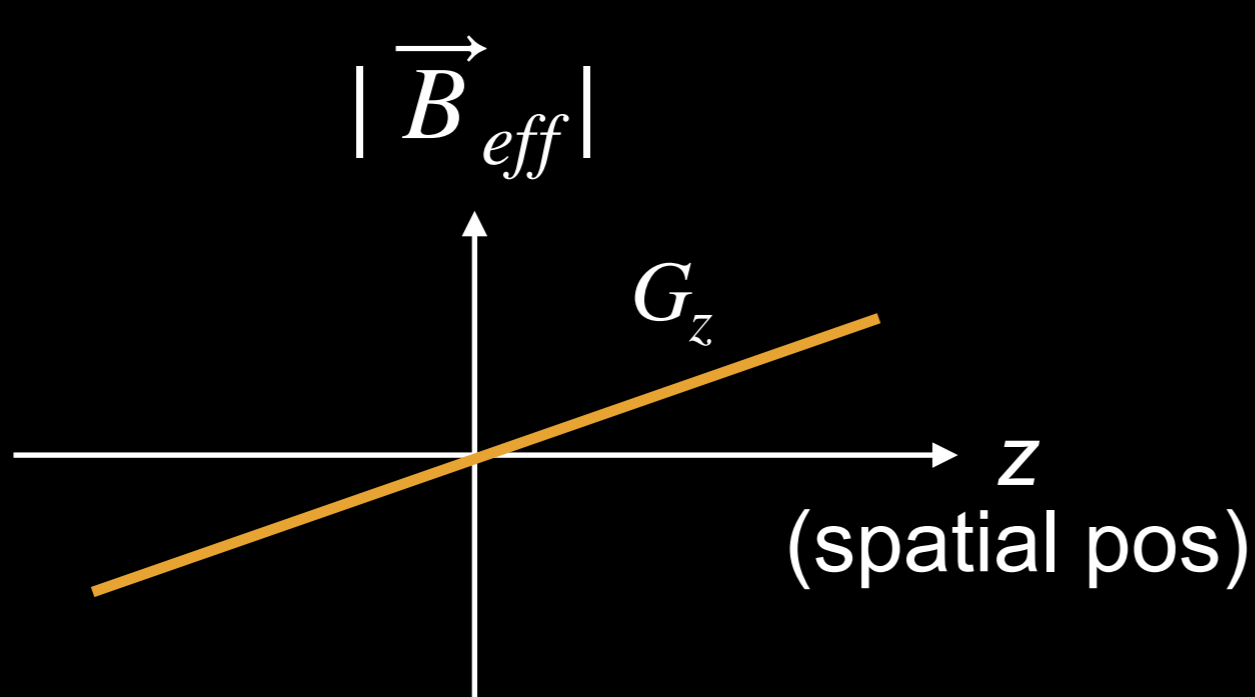
$$\vec{B}_{eff} = \begin{pmatrix} B_1(t) \\ 0 \\ B_0 - \frac{\omega}{\gamma} \end{pmatrix} \rightarrow \vec{B}_{eff} = \begin{pmatrix} B_1(t) \\ 0 \\ B_0 - \frac{\omega}{\gamma} + G_z z \end{pmatrix}$$

Bloch Equation with Gradient

No RF Pulse ($B_1=0$), with G_z on

$$\vec{B} = (B_0 + G_z \cdot z)\hat{k} \quad \vec{B}_{eff} = (B_0 + G_z \cdot z - \frac{\omega_{RF}}{\gamma})\hat{k}$$

On resonance: $\omega_{RF} = \omega_0$, $\vec{B}_{eff} = (G_z \cdot z)\hat{k}$



Bloch Equation (at on-resonance)

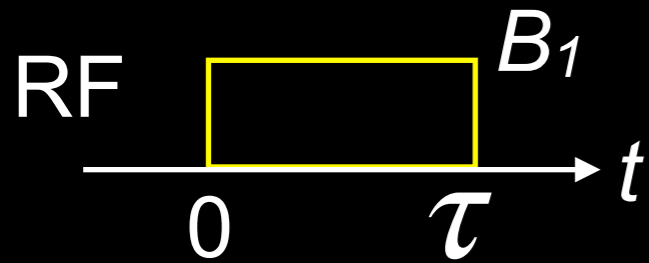
$$\frac{d\vec{M}_{rot}}{dt} = \vec{M}_{rot} \times \gamma \vec{B}_{eff}$$

where $\vec{B}_{eff} = \begin{pmatrix} B_1(t) \\ 0 \\ \cancel{B_0} - \frac{\omega}{\gamma} + G_z z \end{pmatrix}$

$$\frac{d\vec{M}}{dt} = \begin{pmatrix} 0 & \omega(z) & 0 \\ -\omega(z) & 0 & \omega_1(t) \\ 0 & -\omega_1(t) & 0 \end{pmatrix} \vec{M}$$

$$\omega(z) = \gamma G_z z \quad \omega_1(t) = \gamma B_1(t)$$

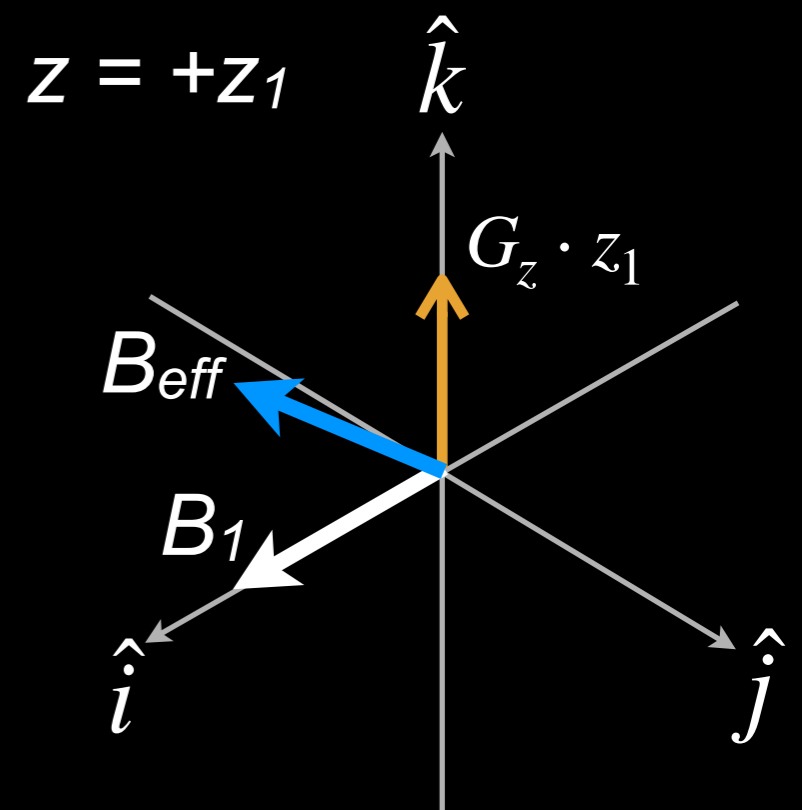
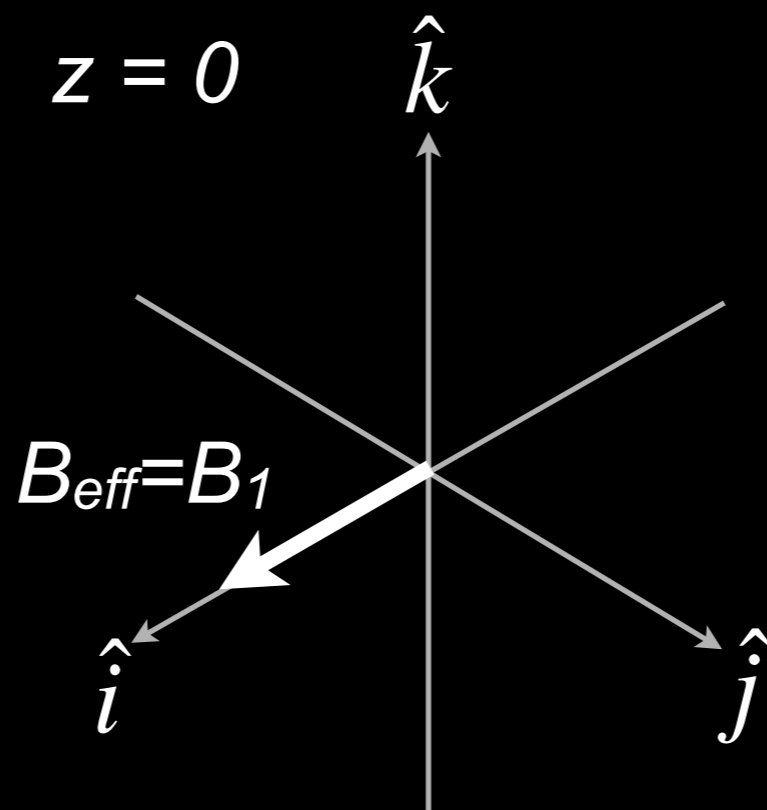
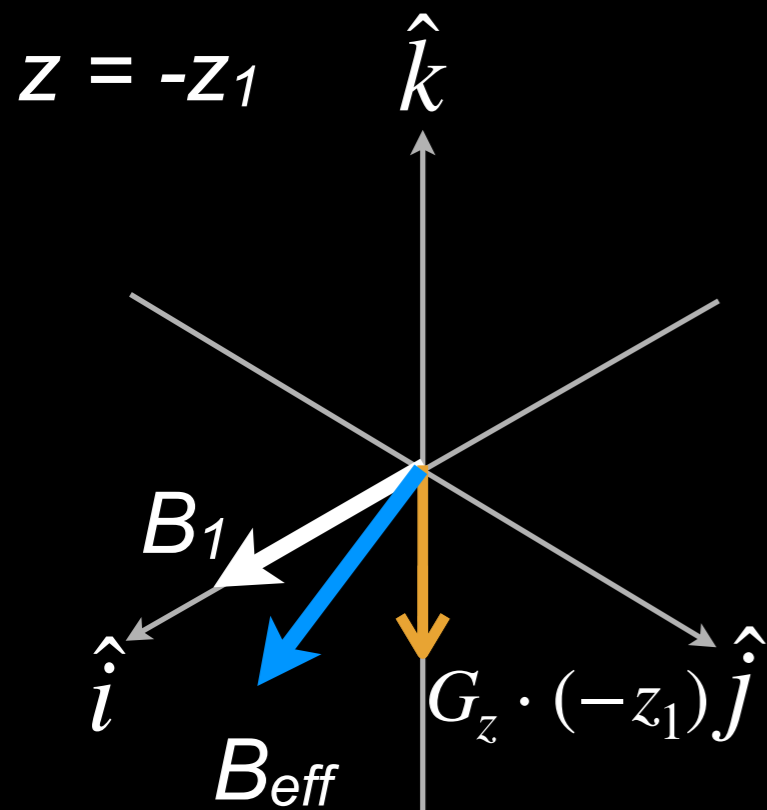
Bloch Equation (at on-resonance)



$$\vec{B}_{eff} = (B_0 + G_z \cdot z - \frac{\omega_{RF}}{\gamma}) \hat{k} + B_1 \hat{i}$$

On resonance: $\omega_{RF} = \omega_0$

$$\vec{B}_{eff} = (G_z \cdot z) \hat{k} + B_1 \hat{i}$$



What happens when z is very far from $z=0$?

B₁ Variations

- In MRI, the B₁ field is not always uniform across the imaging volume
- B₁ inhomogeneity can cause:
 - Image shading
 - Incomplete saturation (e.g. in fat suppression)
 - Incomplete inversion (e.g. CSF suppression, myocardium suppression in cardiac scar imaging)
 - Inaccurate/imprecise quantification in T₁ mapping

B_1 Variations

- It is highly desirable if we can excite tissue homogeneously and produce a uniform flip angle throughout

→ Adiabatic Pulses!

“Adiabatic pulses are a special class of RF pulses that can excite, refocus or invert magnetization vectors uniformly, even in the presence of a spatially nonuniform B_1 field.”

Adiabatic Passage Principle

Adiabatic Pulses

- A special class of RF pulses that can achieve uniform flip angle
- Flip angle is independent of the applied B_1 field

$$\theta \neq \int_0^T B_1(\tau) d\tau$$

- Slice profile of an adiabatic pulse is obtained using Bloch simulations
- Can be used for excitation, inversion and refocusing

Adiabatic vs. Non-Adiabatic Pulses

Adiabatic Pulses:

$$\theta \neq \int_0^T B_1(\tau) d\tau$$

- Amplitude and frequency/phase modulation
- Long duration (8-12 ms)
- Higher B_1 amplitude ($>12 \mu\text{T}$)
- Generally NOT multi-purpose (inversion pulse cannot be used for refocusing, etc.)

Non-Adiabatic Pulses:

$$\theta = \int_0^T B_1(\tau) d\tau$$

- Amplitude modulation, constant carrier frequency (constant phase)
- Short duration (0.3 ms to 1 ms)
- Lower B_1 amplitude
- Generally multi-purpose

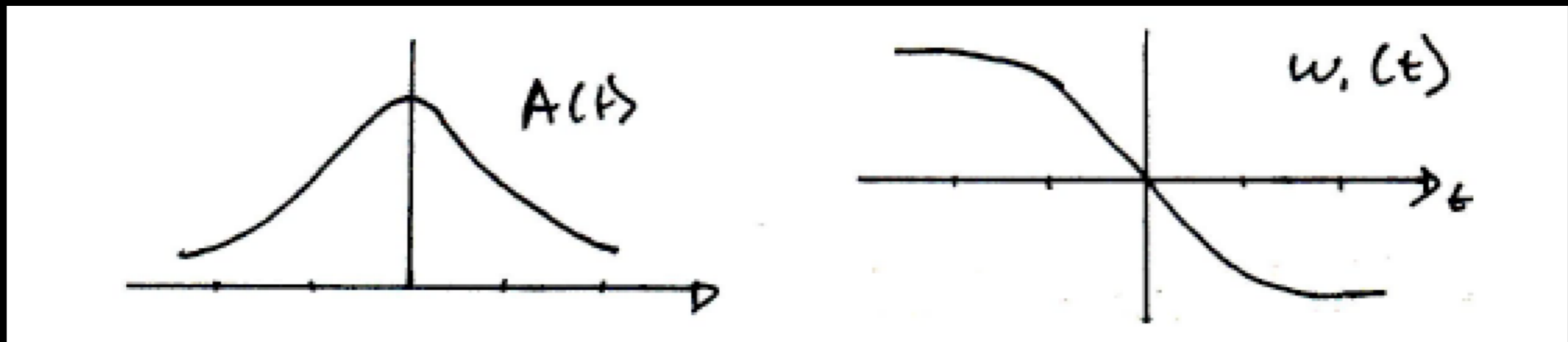
Adiabatic Pulses

- Frequency modulated pulses:

$$B_1(t) = A(t) \exp^{-i \int \omega_1(t') dt'}$$

envelope

frequency sweep



- Or phase modulation:

$$B_1(t) = A(t) \exp^{-i\phi(t)}$$

Bloch Equation (at on-resonance)

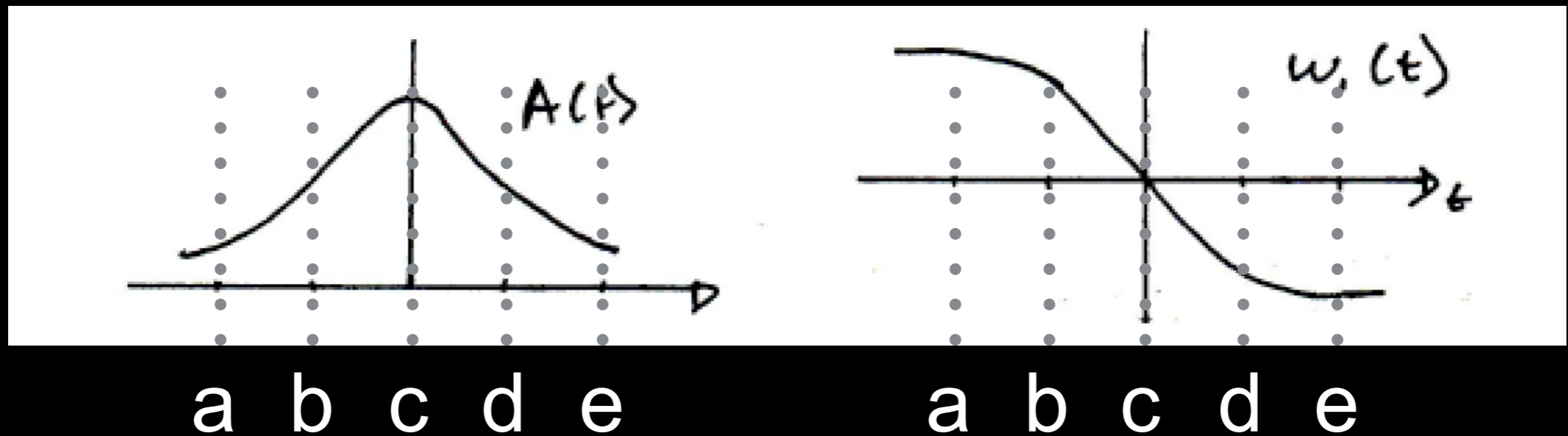
$$B_1(t) = A(t) \exp^{-i \int \omega_1(t') dt'}$$

$$\frac{d\vec{M}}{dt} = \vec{M} \times \gamma \vec{B}_{eff}$$

where $\vec{B}_{eff} = \begin{pmatrix} A(t) \\ 0 \\ \cancel{B_0} + \frac{\omega_1(t)}{\gamma} \end{pmatrix}$

$$\frac{d\vec{M}}{dt} = \begin{pmatrix} 0 & \omega_1(t) & 0 \\ -\omega_1(t) & 0 & \gamma A(t) \\ 0 & -\gamma A(t) & 0 \end{pmatrix} \vec{M}$$

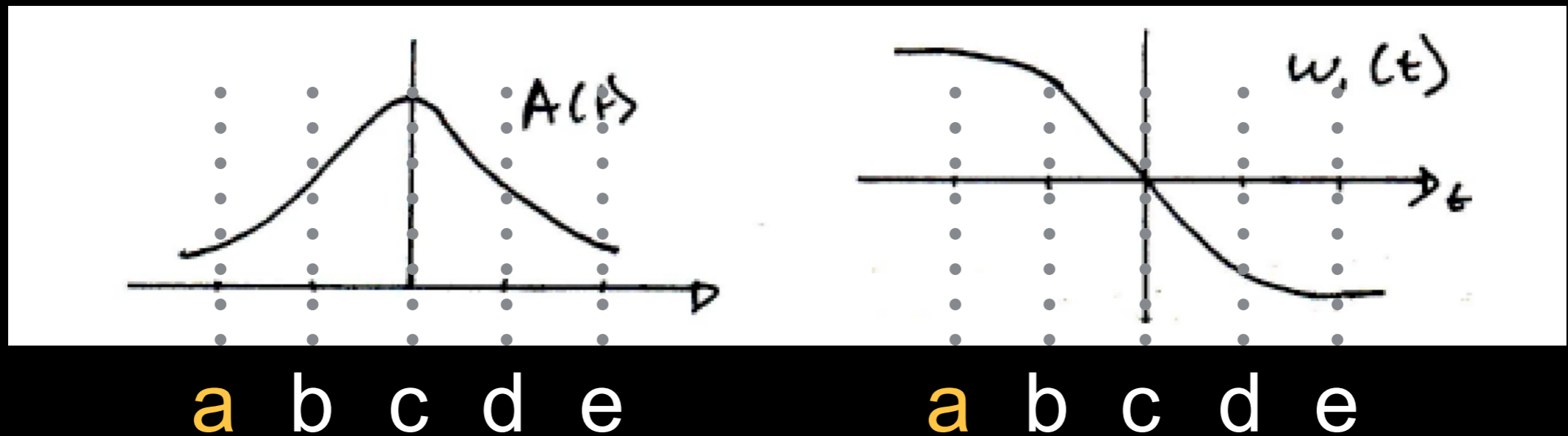
Magnetization Plot



$$B_1(t) = A(t)e^{-i\omega_1(t)\cdot t}$$

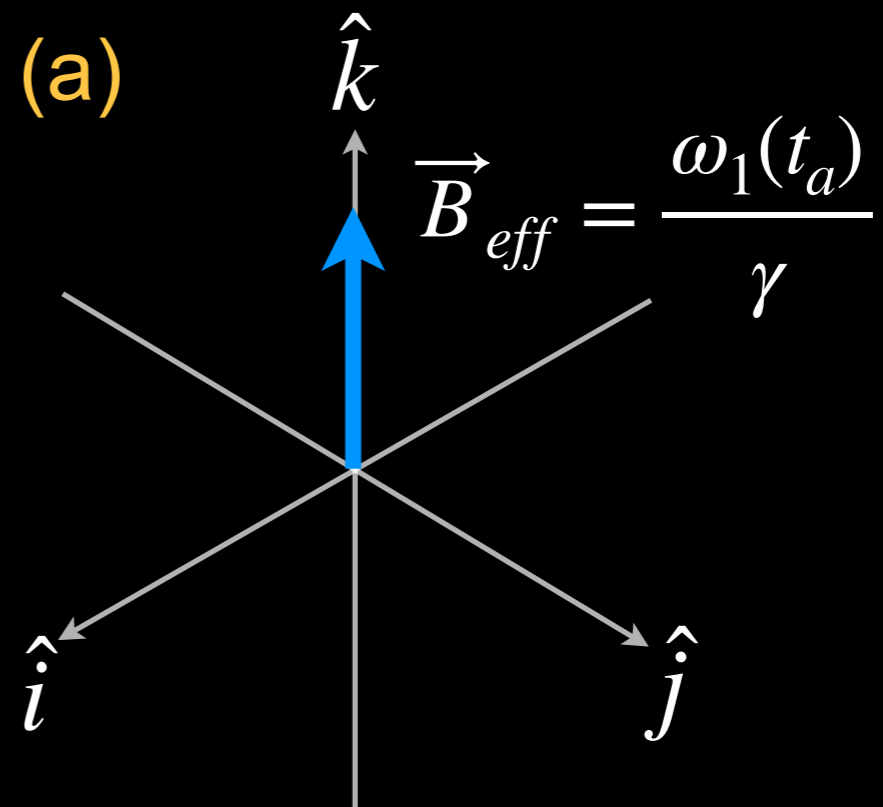
$$\vec{B}_{eff} = \begin{pmatrix} A(t) \\ 0 \\ \frac{\omega_1(t)}{\gamma} \end{pmatrix}$$

Magnetization Plot

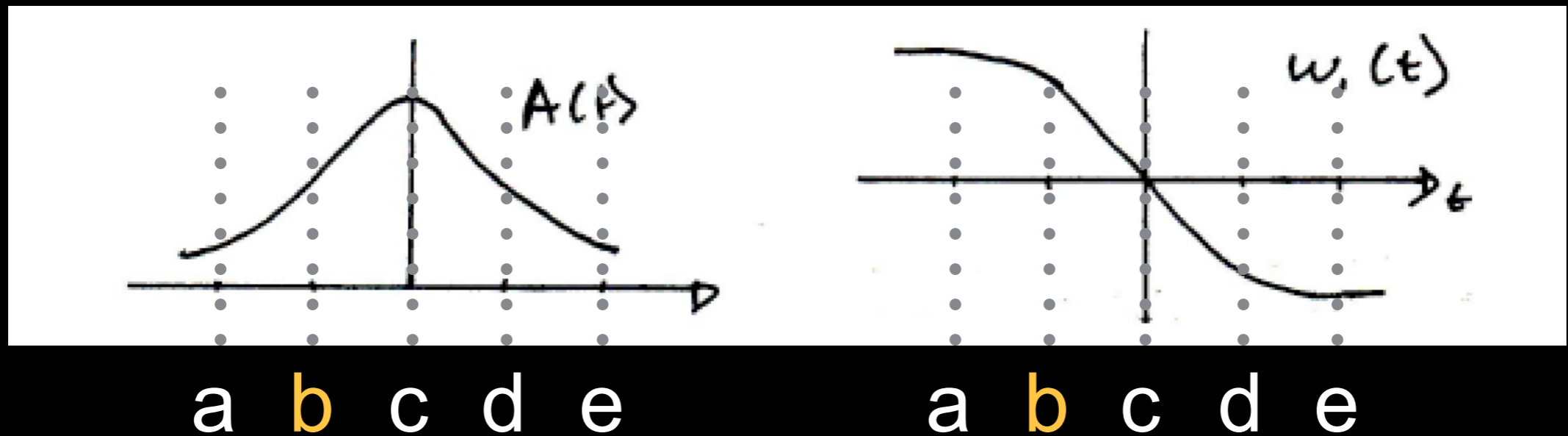


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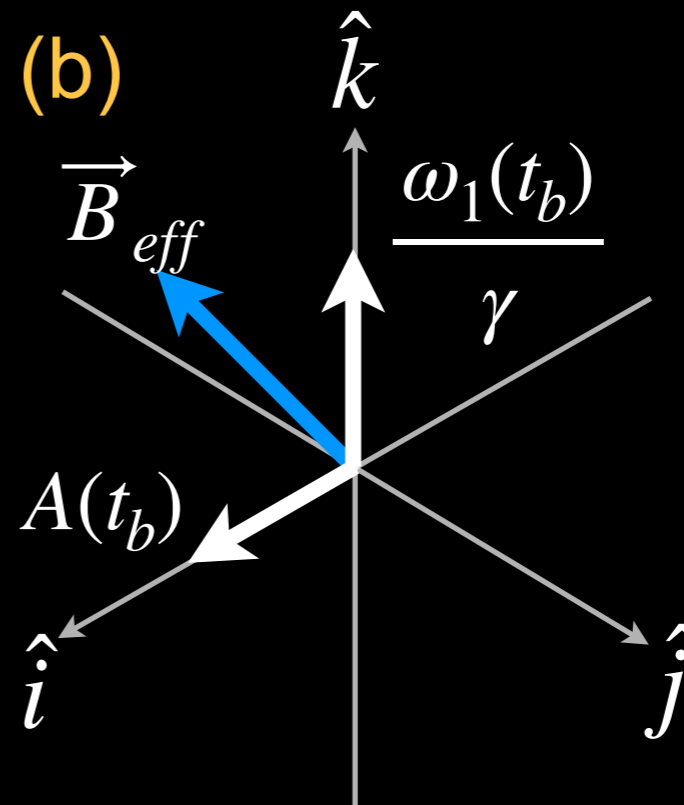


Magnetization Plot

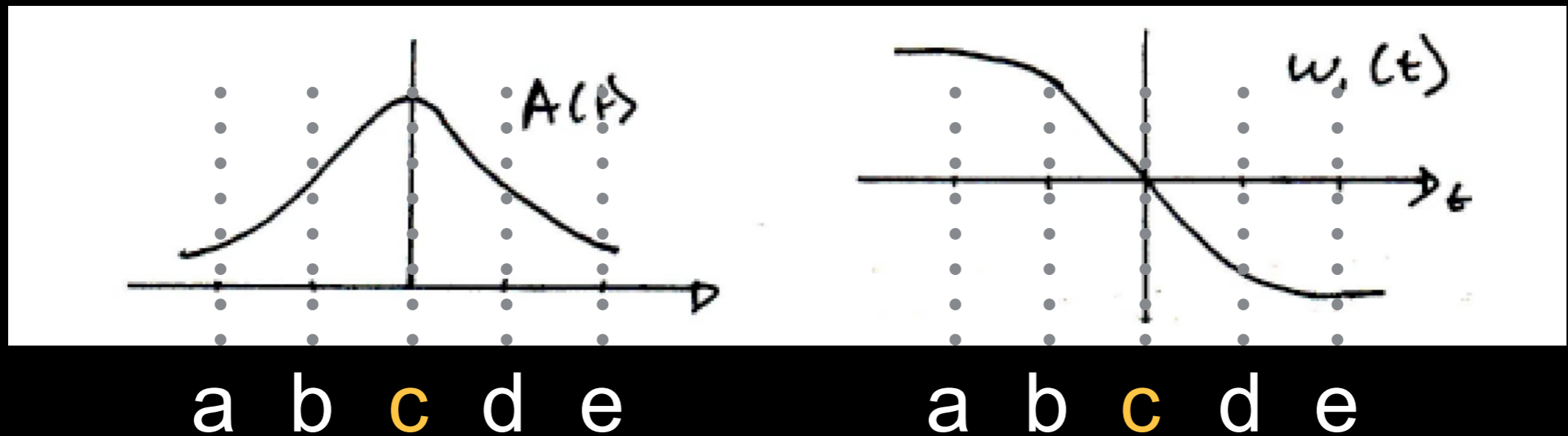


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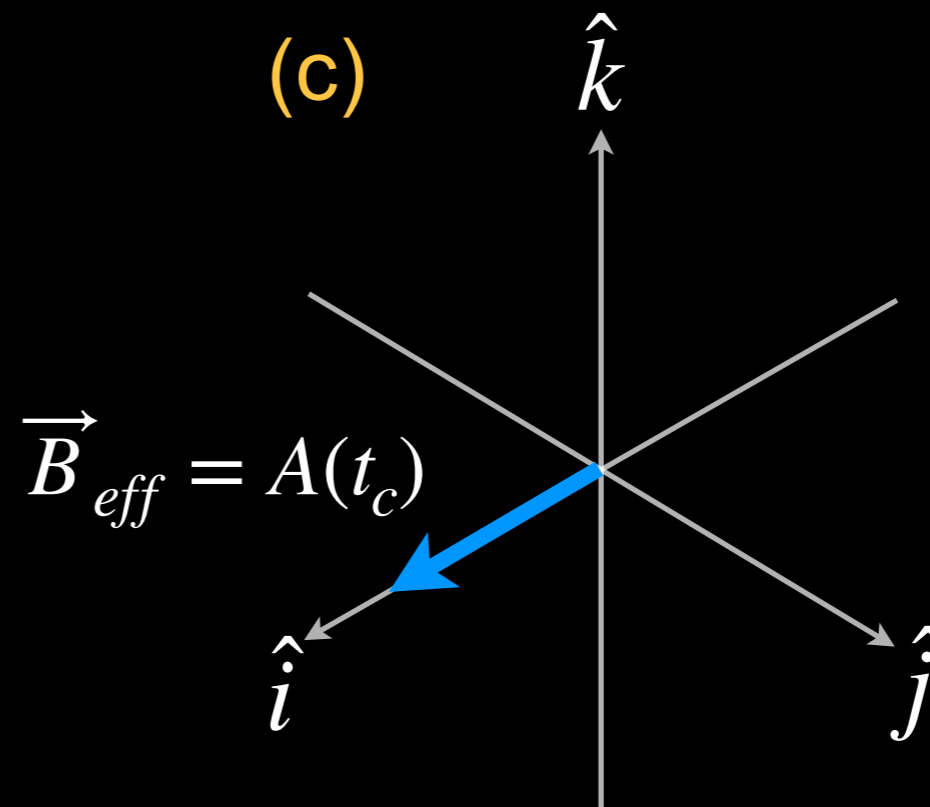


Magnetization Plot

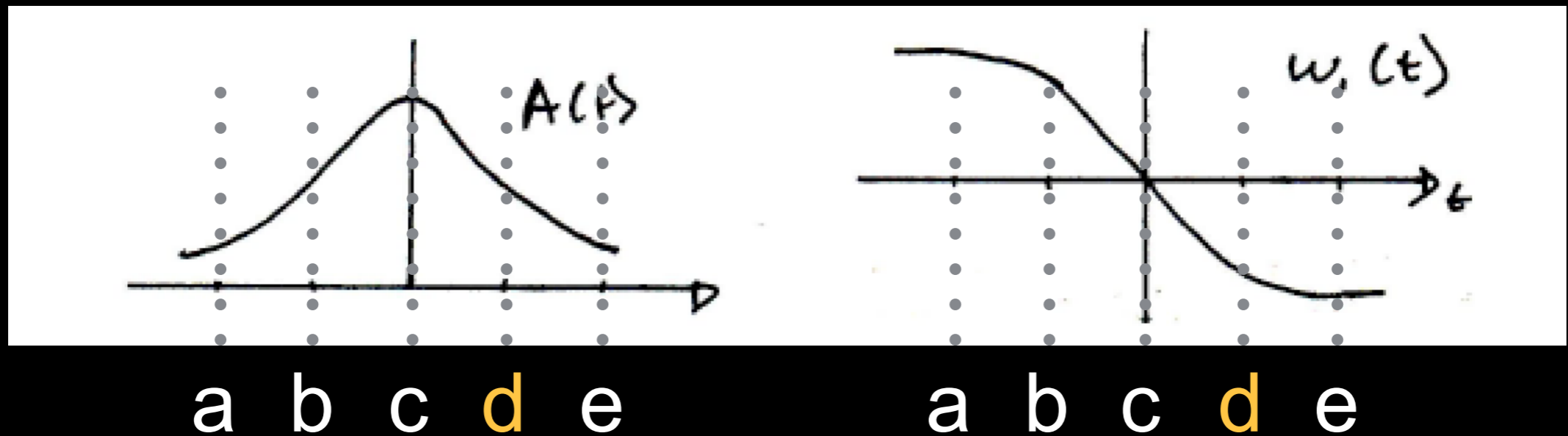


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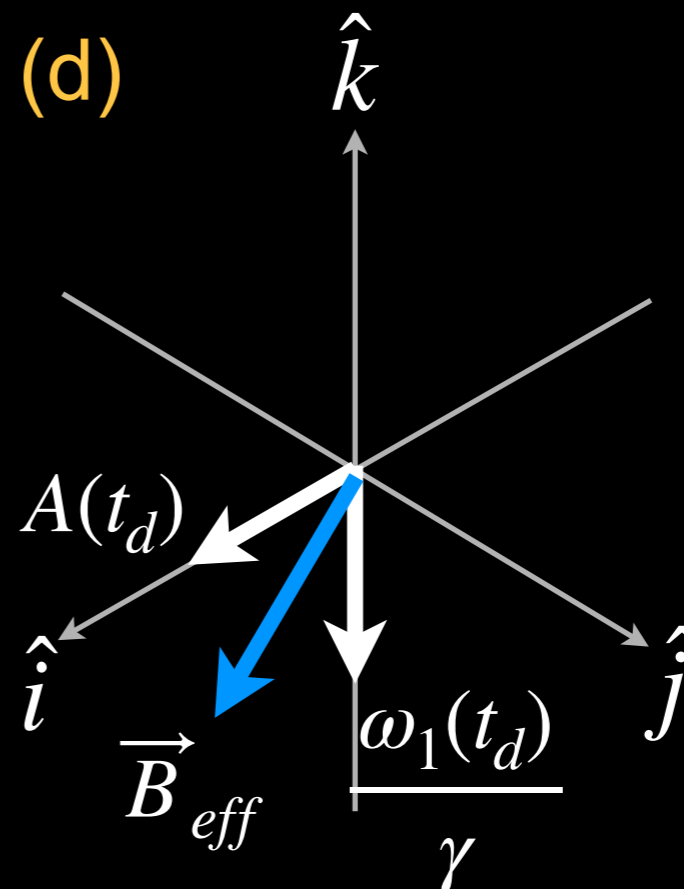


Magnetization Plot

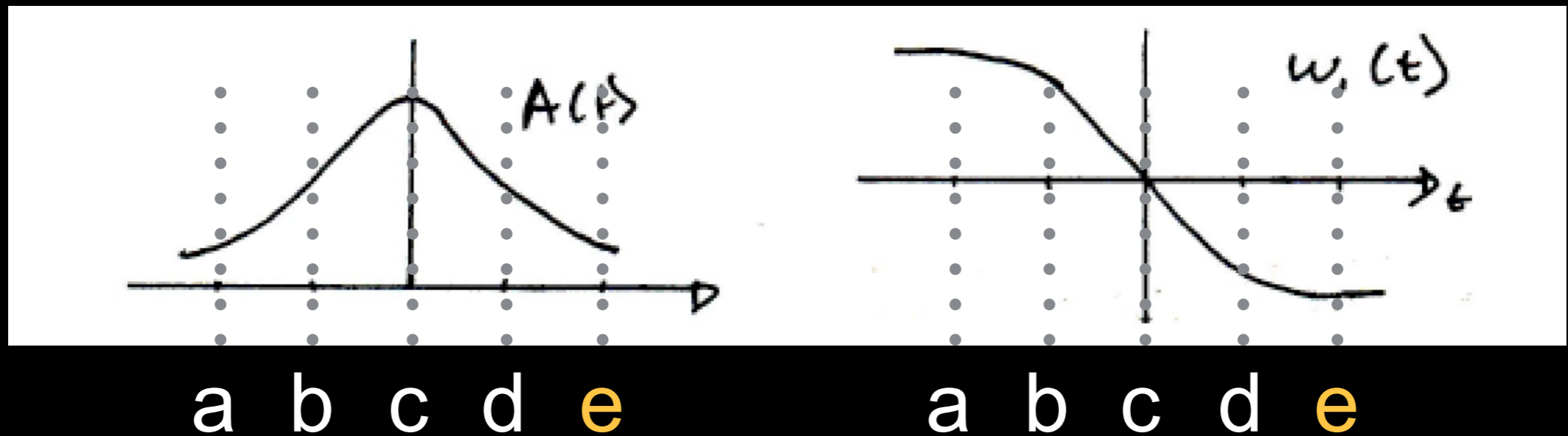


$$B_1(t) = A(t)e^{-i\omega_1(t)\cdot t}$$

$$\vec{B}_{eff} = \begin{pmatrix} A(t) \\ 0 \\ \frac{\omega_1(t)}{\gamma} \end{pmatrix}$$

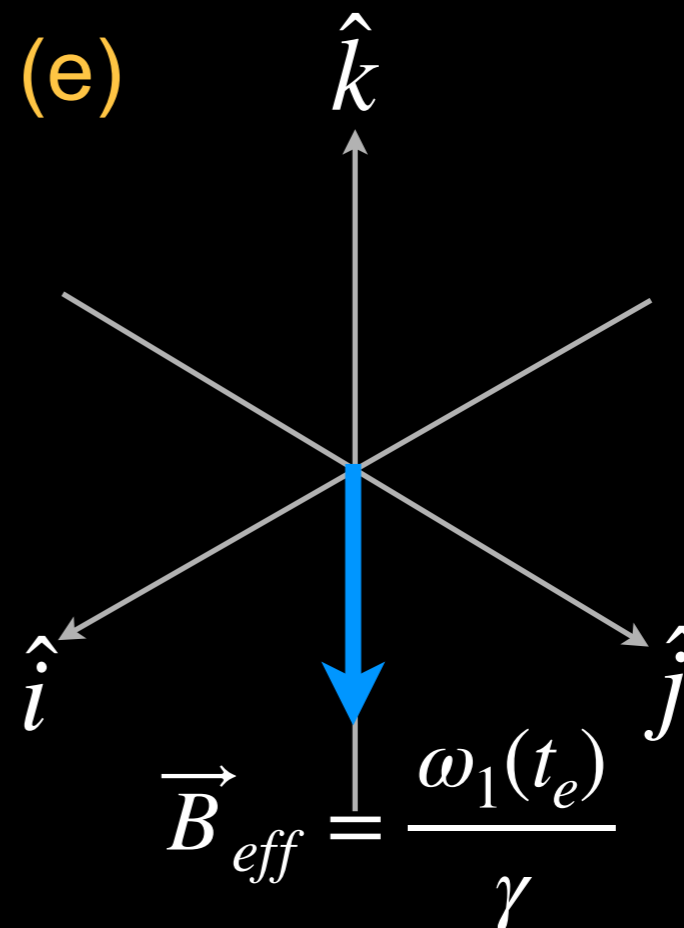


Magnetization Plot

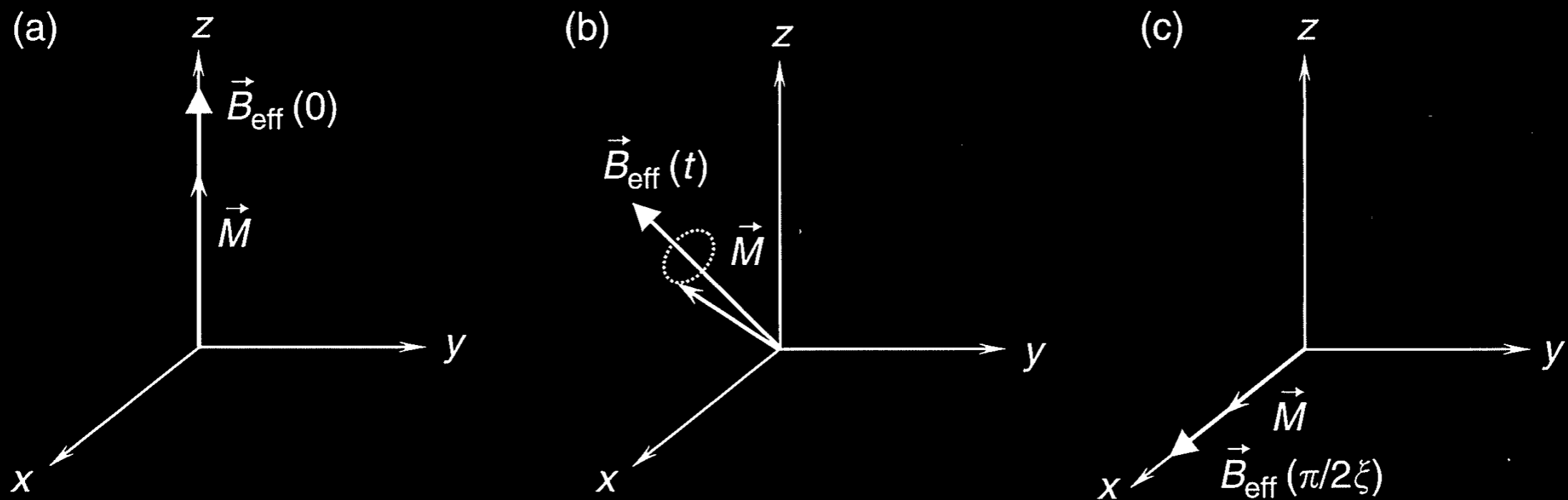
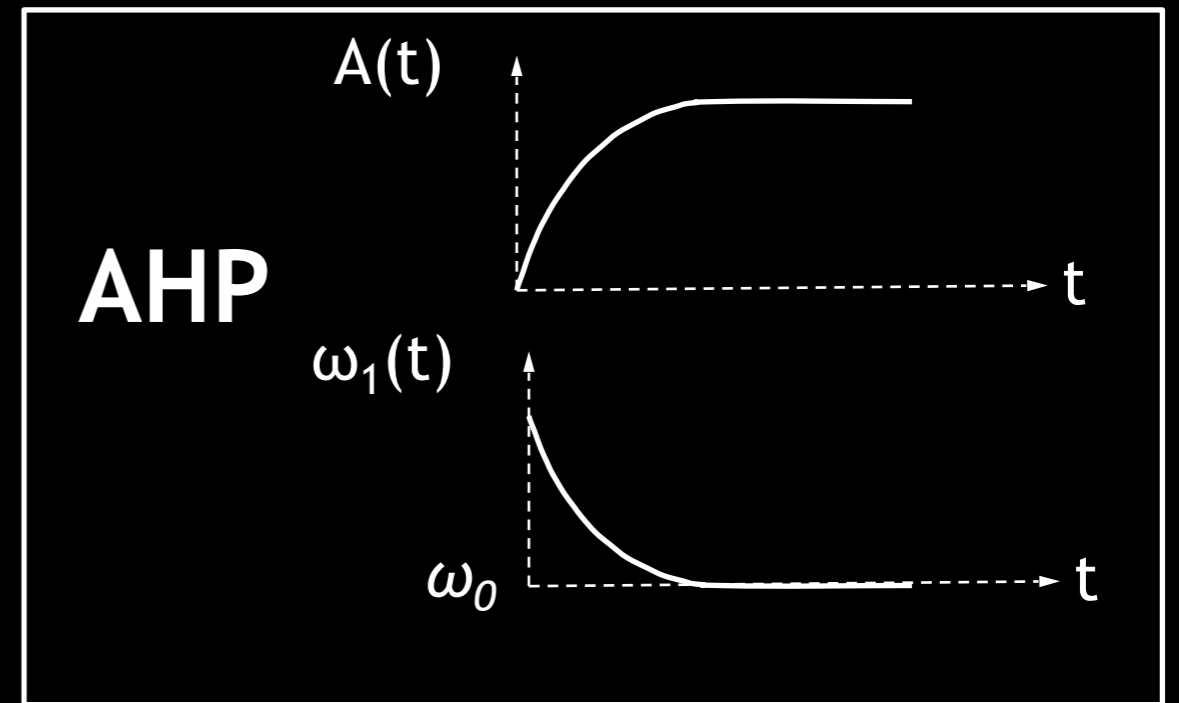


$$B_1(t) = A(t)e^{-i\omega_1(t)\cdot t}$$

$$\vec{B}_{eff} = \begin{pmatrix} A(t) \\ 0 \\ \frac{\omega_1(t)}{\gamma} \end{pmatrix}$$



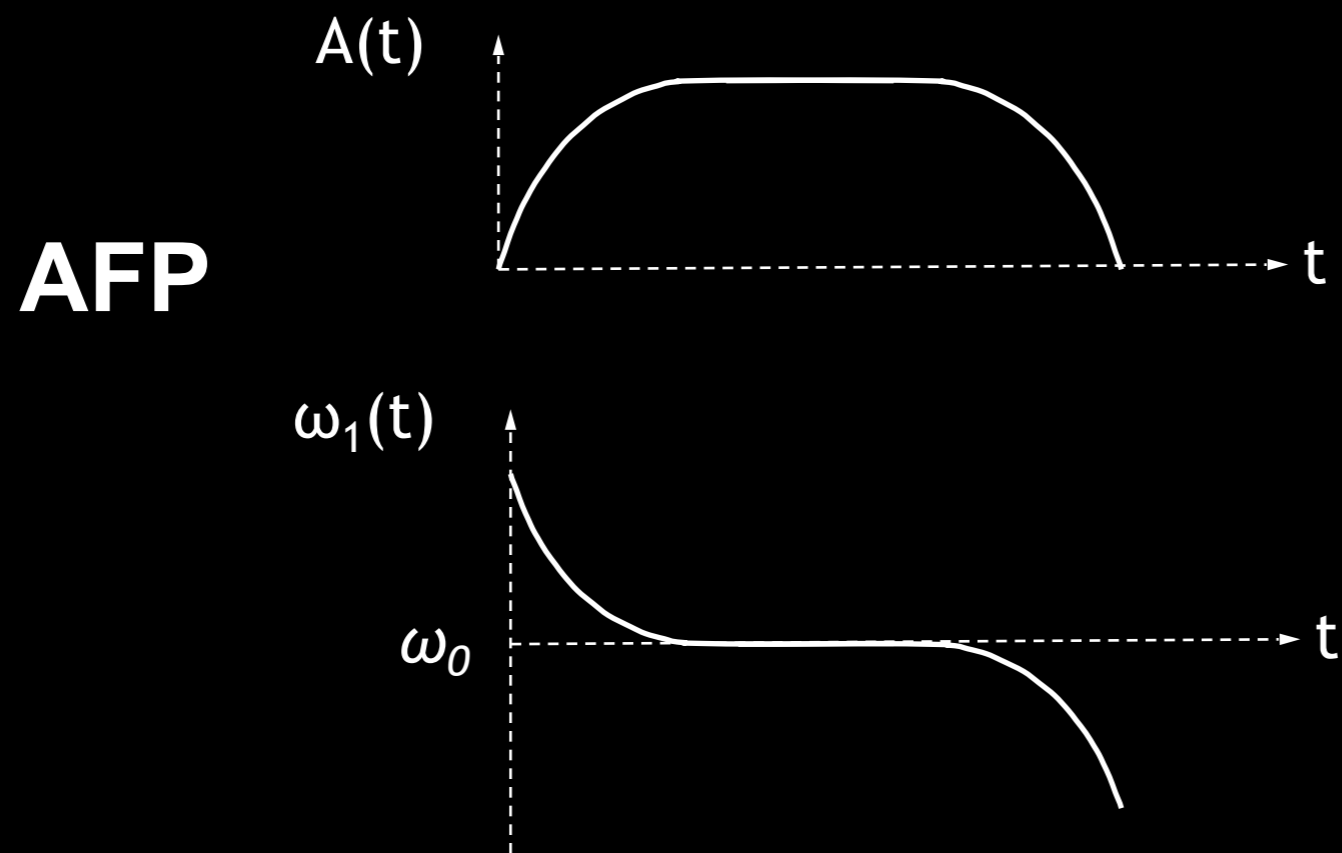
Adiabatic Excitation



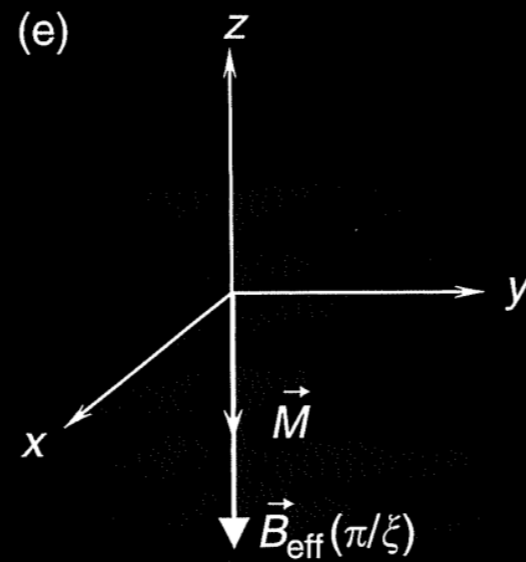
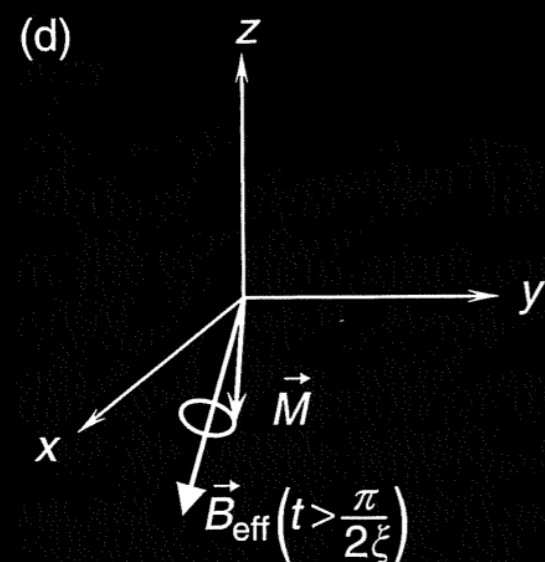
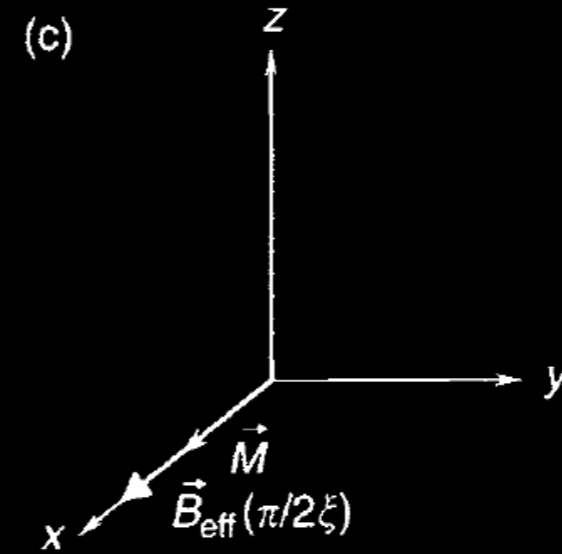
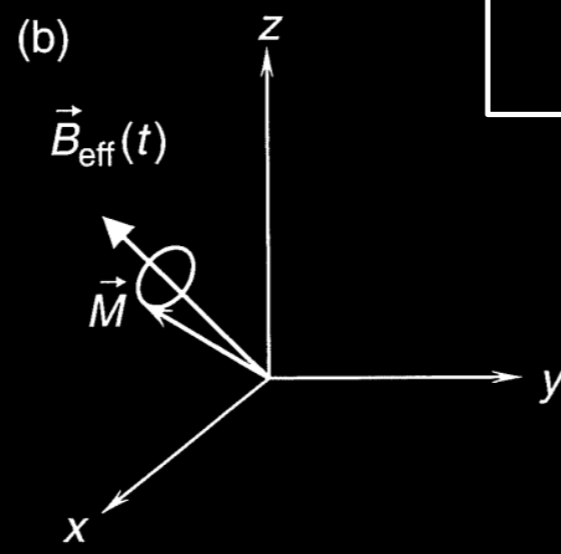
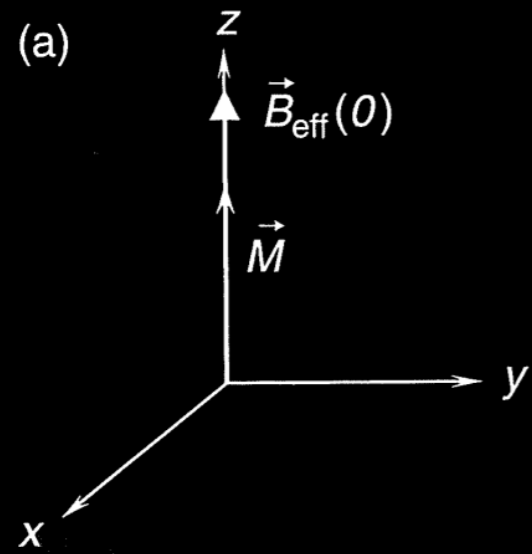
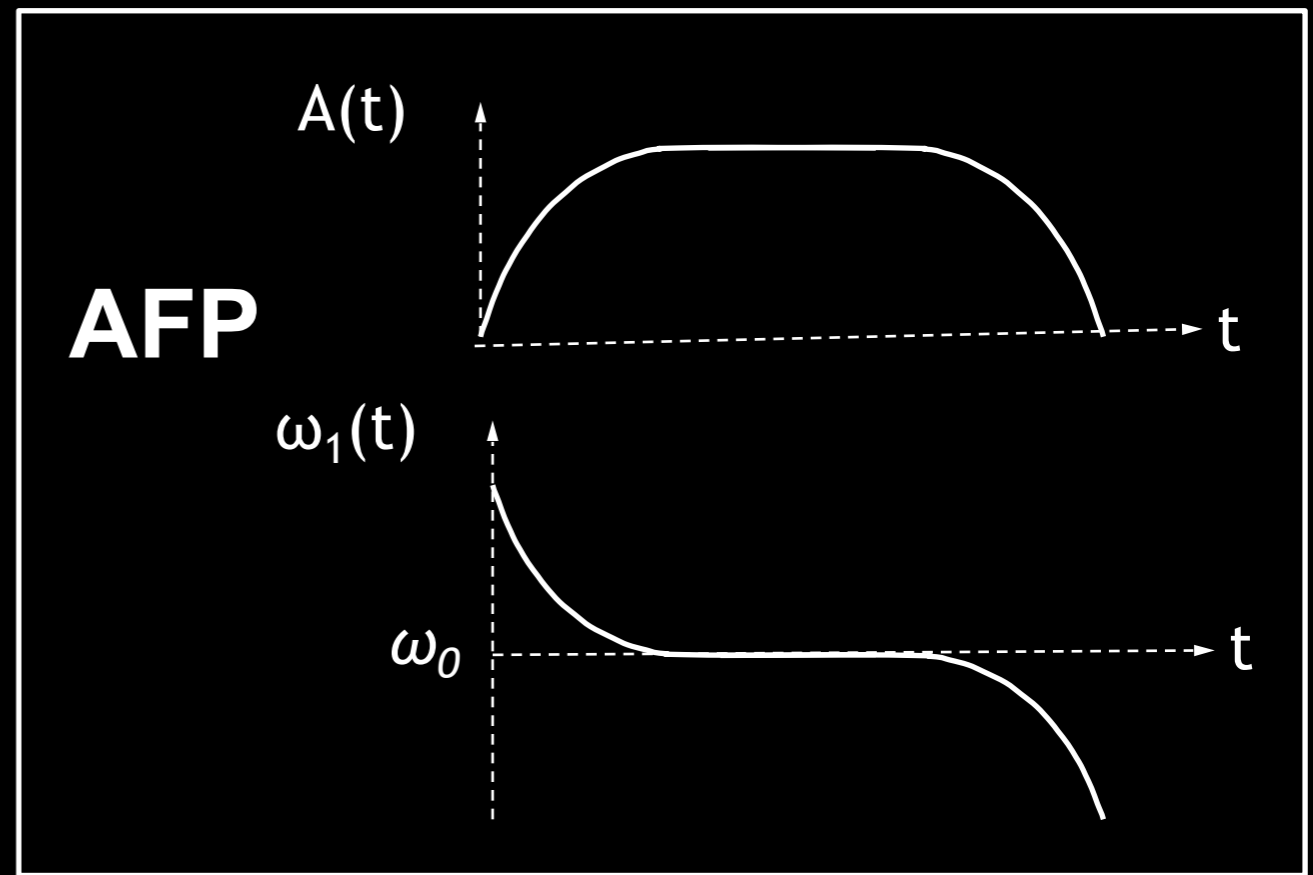
- At the end of the pulse, all the magnetization is in the transverse plane, so we have adiabatic excitation!
- This is also called an **adiabatic half passage (AHP)**

Adiabatic Inversion

- An adiabatic inversion requires an adiabatic full passage (AFP) pulse:



Adiabatic Inversion



Adiabatic Inversion

Design of Adiabatic Inversion

- General equation for an adiabatic pulse:

$$B_1(t) = A(t) \exp^{-i \int \omega_1(t') dt'}$$

- Many different types of adiabatic pulses can be designed by choosing different amplitude and frequency modulation functions
- The most famous one is...

The Hyperbolic Secant Inversion Pulse!

Hyperbolic Secant Pulse Equations

$$B_1(t) = A(t) \exp^{-i \int \omega_1(t') dt'}$$

where

$$A(t) = A_0 \operatorname{sech}(\beta t)$$

$$\omega_1(t) = -\mu\beta \tanh(\beta t)$$

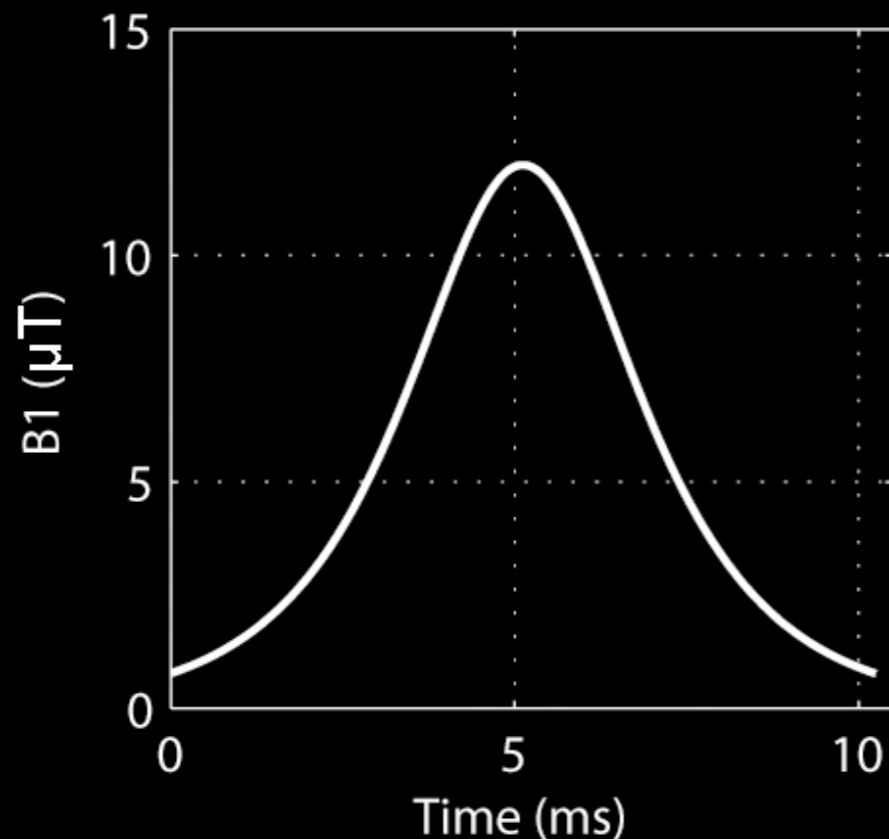
A_0 : peak amplitude (μT)

β : frequency modulation parameter (rad/s)

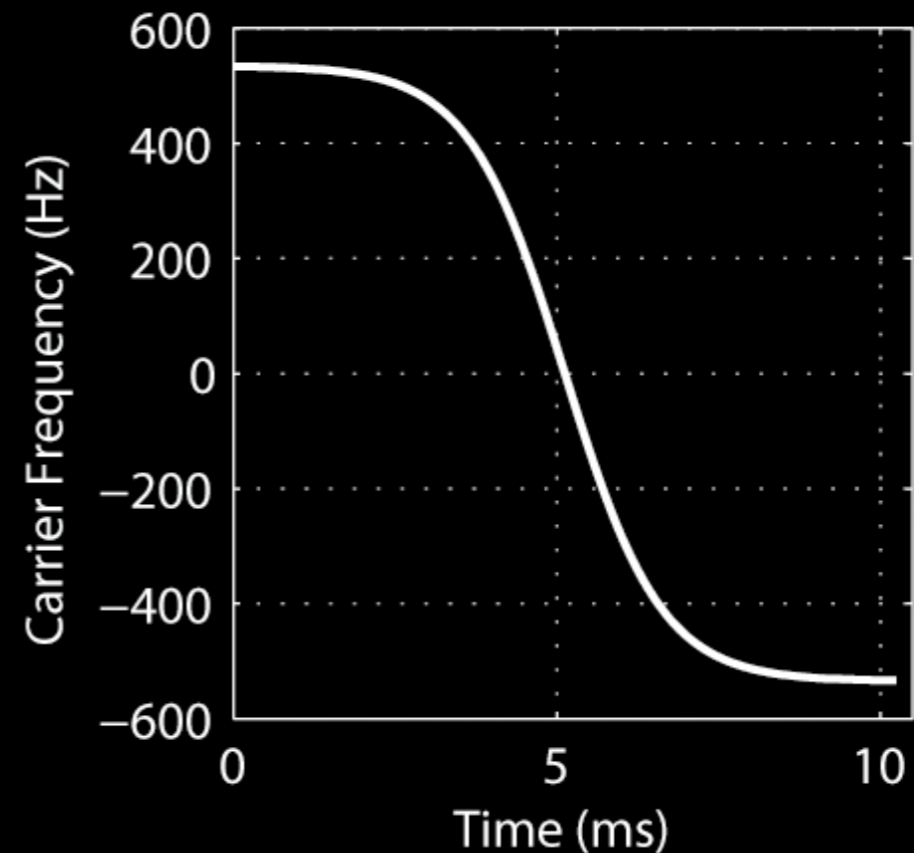
μ : phase modulation parameter (dimensionless)

Hyperbolic Secant Pulse Example

Amplitude Modulation, $A(t)$



Frequency Modulation, $\omega_1(t)$



Pulse Parameters:

$$A_0 = 12 \mu T$$

$$\mu = 5$$

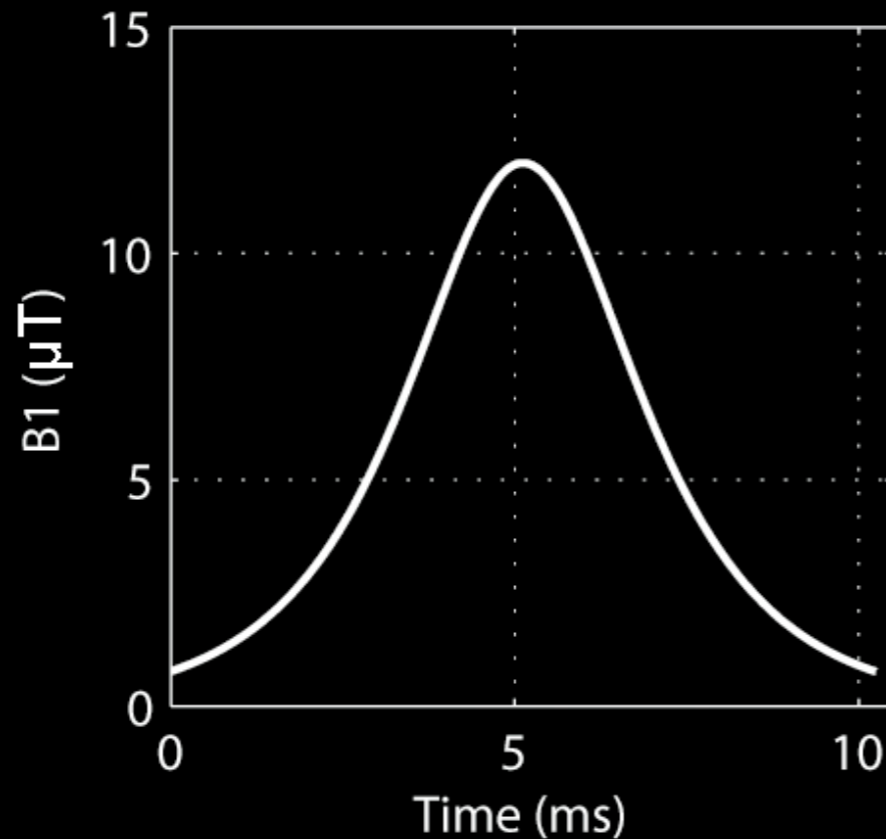
$$\beta = 672 \text{ rad/s}$$

$$\text{Duration} = 10.24 \text{ ms}$$

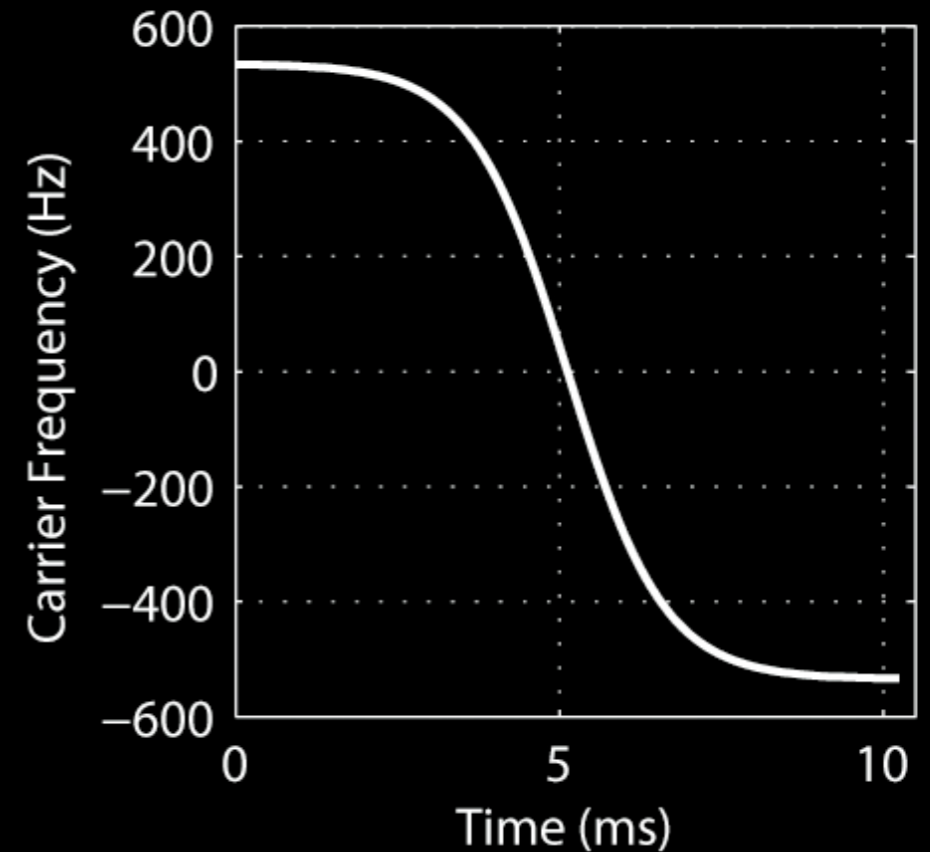
Comparing Hyperbolic Secant with an AFP Example

Hyperbolic Secant Pulse

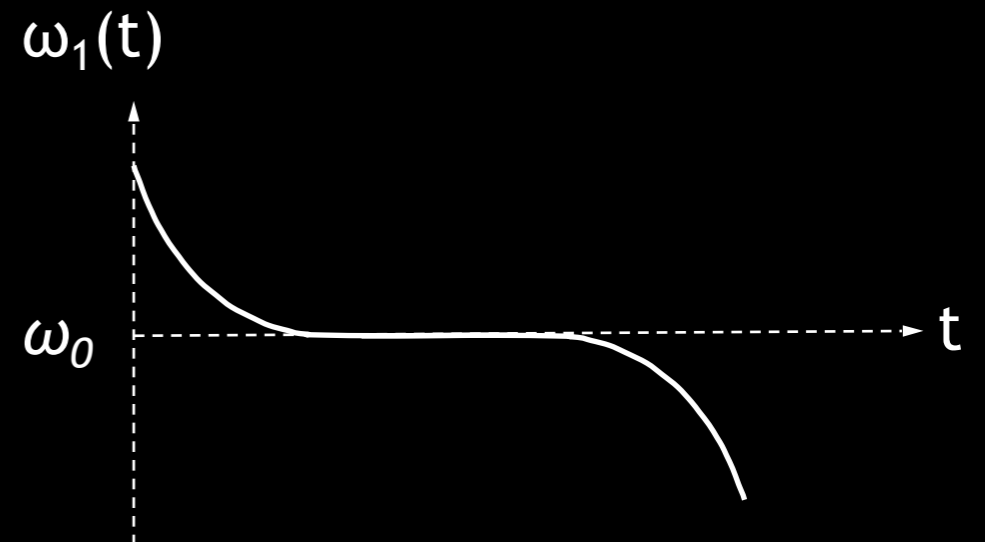
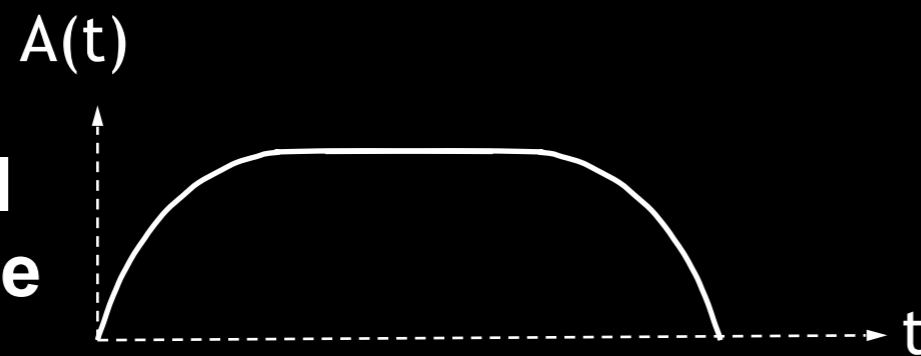
Amplitude Modulation, $A(t)$



Frequency Modulation, $\omega_1(t)$



General Adiabatic Full Passage pulse



Some Examples of Other Adiabatic Inversion Pulses

| Pulse Name | $A(t)$ | $\omega_1(t)$ |
|-------------------------------|---|--|
| Lorentz | $\frac{1}{1+\beta\tau^2}$ | $\frac{\tau}{1+\beta\tau^2} + \frac{1}{\sqrt{\beta}} \tan^{-1}(\sqrt{\beta}\tau)$ |
| HS | $\text{sech}(\beta\tau)$ | $\frac{\tanh(\beta\tau)}{\tanh(\beta)}$ |
| Gauss ^c | $\exp\left(-\frac{\beta^2\tau^2}{2}\right)$ | $\frac{\text{erf}(\beta\tau)}{\text{erf}(\beta)}$ |
| Hanning | $\frac{1+\cos(\pi\tau)}{2}$ | $\tau + \frac{4}{3\pi} \sin(\pi\tau) \left[1 + \frac{1}{4} \cos(\pi\tau) \right]$ |
| HSn ^c ($n=8$) | $\text{sech}(\beta\tau^n)$ | $\int \text{sech}^2(\beta\tau^n) d\tau$ |
| Sin40 ^d ($n=40$) | $1 - \left \sin^n\left(\frac{\pi\tau}{2}\right) \right $ | $\tau - \int \sin^n\left(\frac{\pi\tau}{2}\right) \left(1 + \cos^2\left(\frac{\pi\tau}{2}\right) \right) d\tau$ |

Some Examples of Other Adiabatic Inversion Pulses

| Pulse Name | $A(t)$ | $\omega_1(t)$ |
|------------|---------------------------|---|
| Lorentz | $\frac{1}{1+\beta\tau^2}$ | $\frac{\tau}{1+\beta\tau^2} + \frac{1}{\sqrt{\beta}} \tan^{-1}(\sqrt{\beta}\tau)$ |
| HS | $\text{sech}(\beta\tau)$ | $\frac{\tanh(\beta\tau)}{\tanh(\beta)}$ |

The shape of the inversion profile depends on the choice $A(t)$ and $\omega_1(t)$!

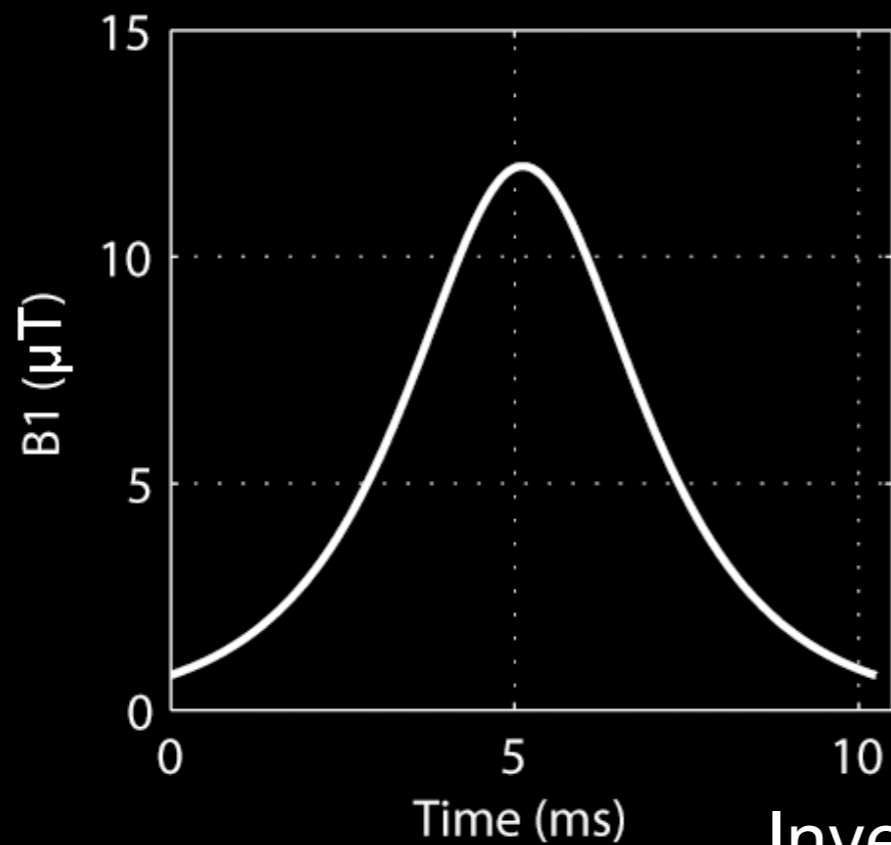
HSn^c ($n=8$) $\text{sech}(\beta\tau^n)$ $\int \text{sech}^2(\beta\tau^n) d\tau$

Sin40^d ($n=40$) $1 - \left| \sin^n\left(\frac{\pi\tau}{2}\right) \right|$ $\tau - \int \sin^n\left(\frac{\pi\tau}{2}\right) \left(1 + \cos^2\left(\frac{\pi\tau}{2}\right)\right) d\tau$

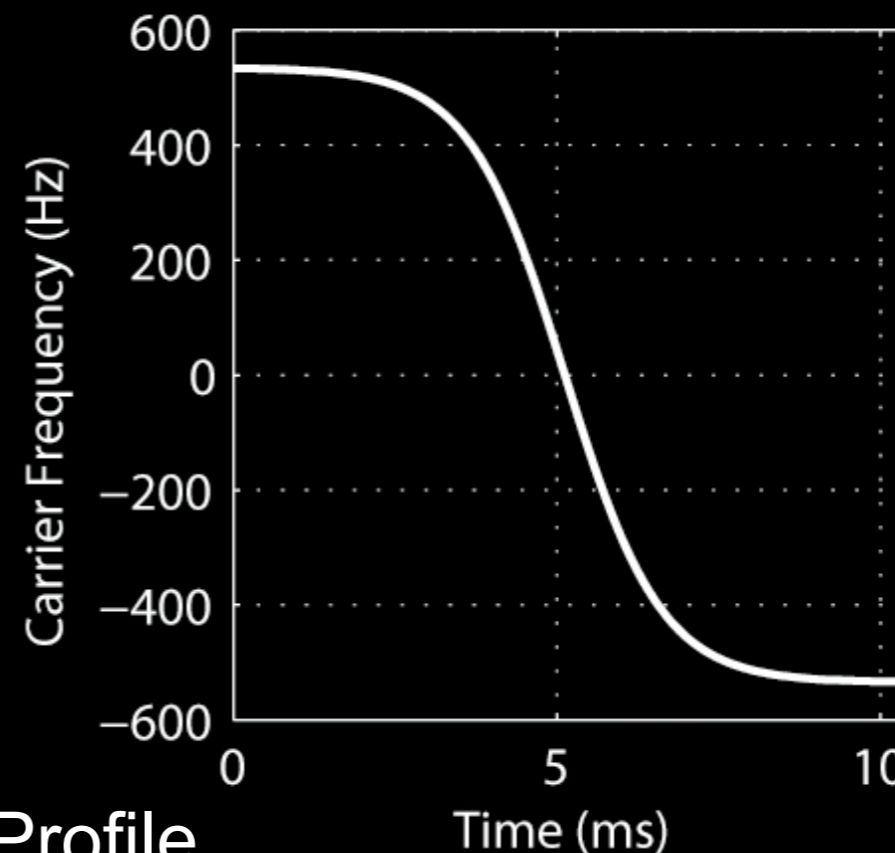
What Will Inversion Profile Look Like?

Hyperbolic Secant
Pulse

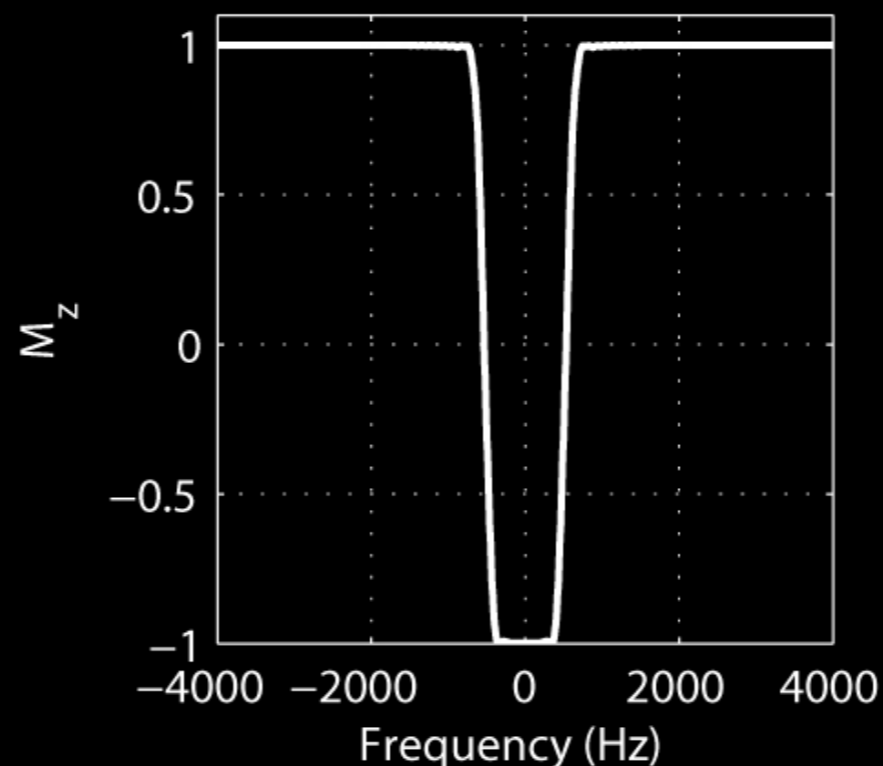
Amplitude Modulation, $A(t)$



Frequency Modulation, $\omega_1(t)$



Inversion Profile



Inversion Profiles

- The inversion profile typically calculated using Bloch simulation of the RF pulse (will be covered later) shows us the inversion efficiency and RF bandwidth
- The inversion efficiency depends strongly on the B_1 amplitude (as well as pulse duration, T_1 , T_2 and pulse shape)
- For the hyperbolic secant pulse,

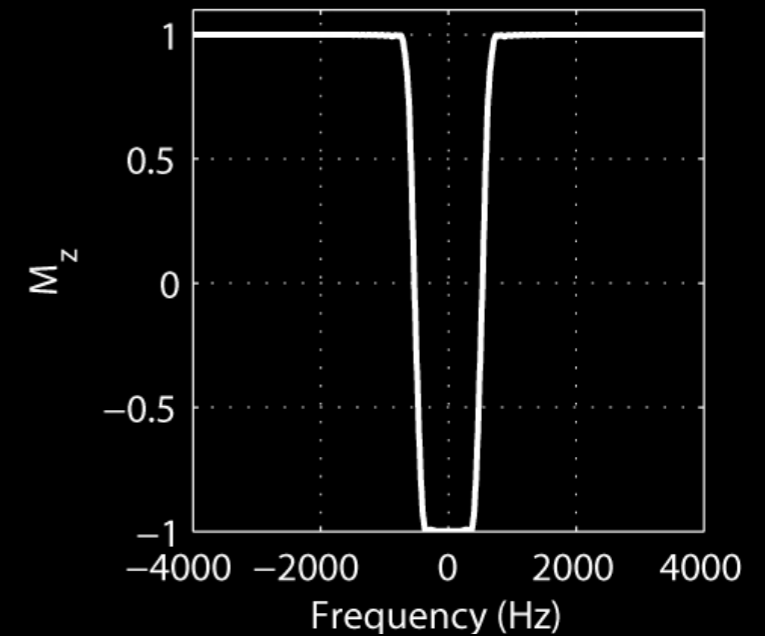
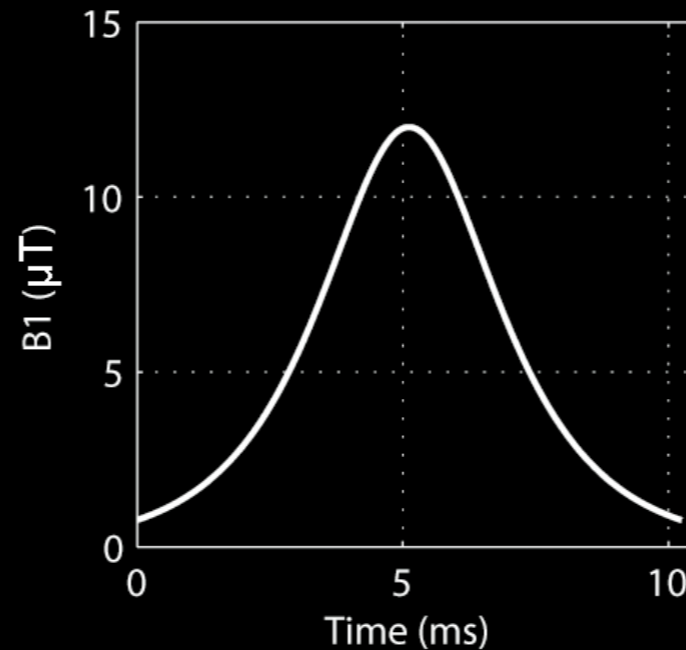
$$\text{RF spectral bandwidth} = \mu\beta$$

$$B_{1\text{max}} \gg (\beta\sqrt{\mu})/\gamma \quad (B_1 \text{ threshold for adiabaticity})$$

Hyperbolic Secant: Adiabatic Property

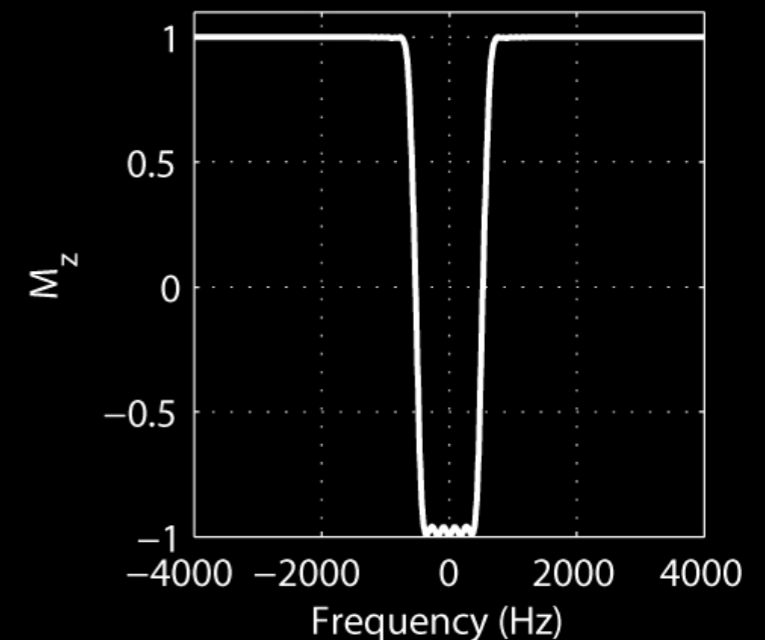
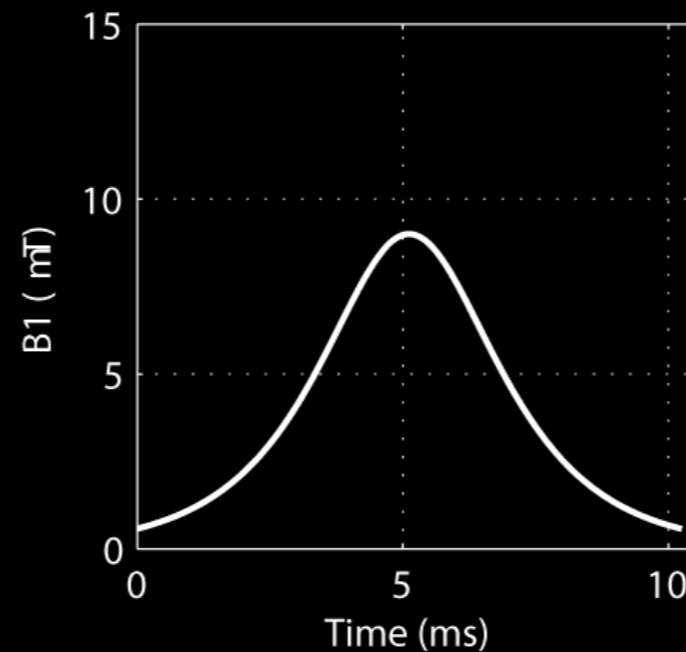
Original Pulse (100%)

$$B_{1\max} = 12 \mu\text{T}$$



75% Attenuated Pulse

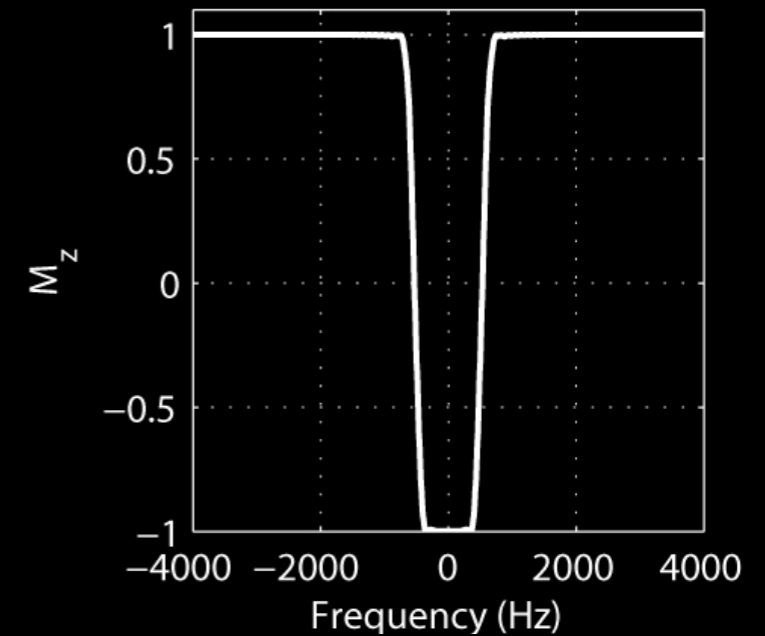
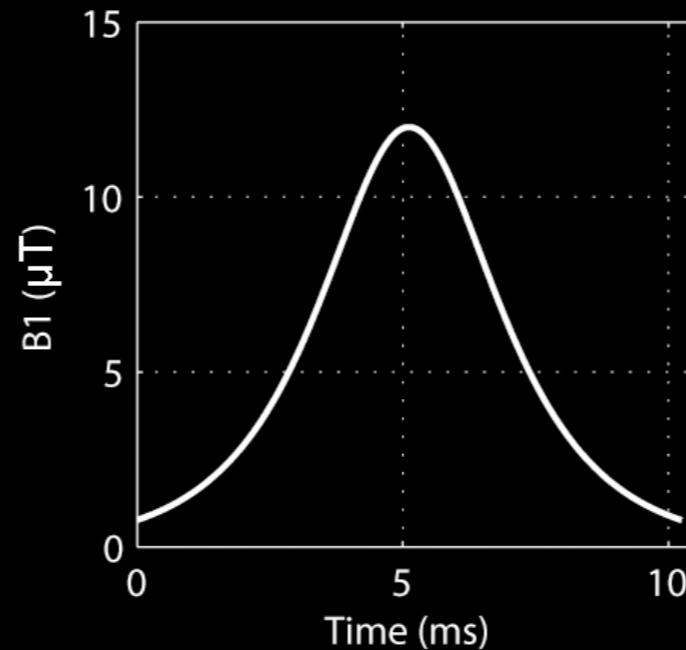
$$B_{1\max} = 9 \mu\text{T}$$



Hyperbolic Secant: Adiabatic Property

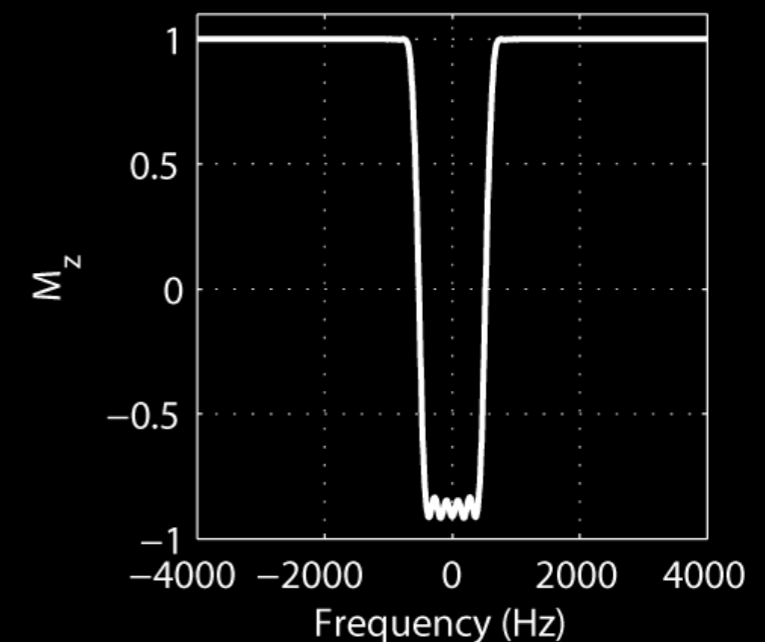
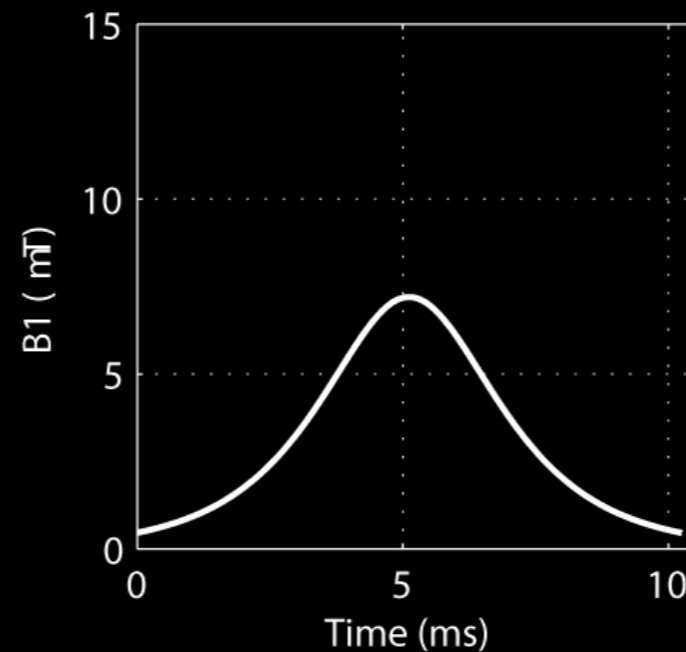
Original Pulse (100%)

$$B_{1\max} = 12 \mu\text{T}$$



60% Attenuated Pulse

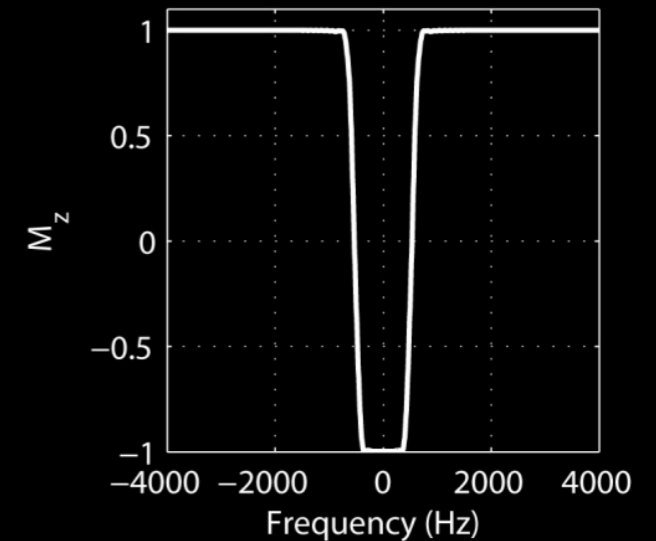
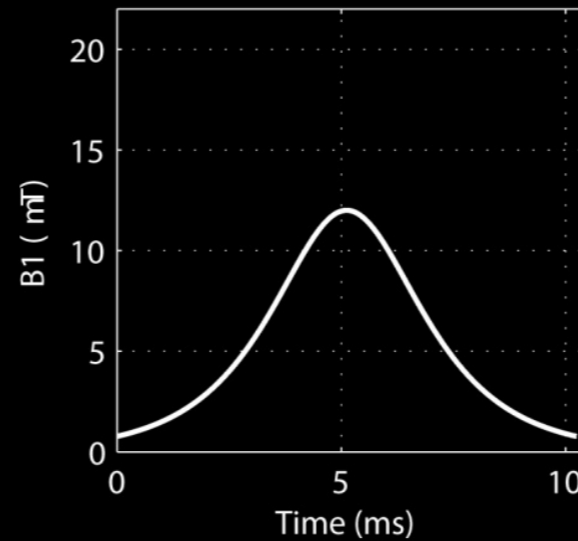
$$B_{1\max} = 7.2 \mu\text{T}$$



B₁ Threshold ≈ 6 μT

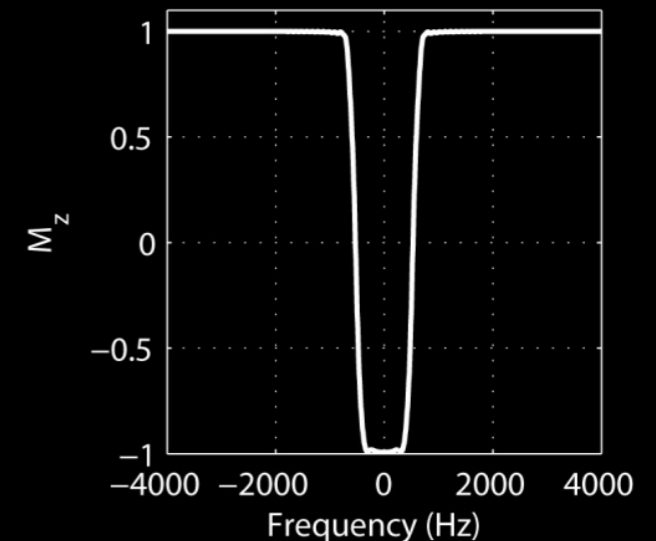
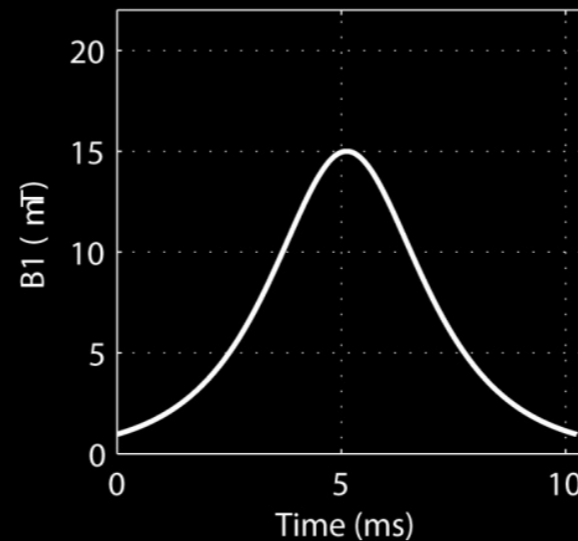
Original Pulse (100%)

$$B_1 = 12 \mu\text{T}$$



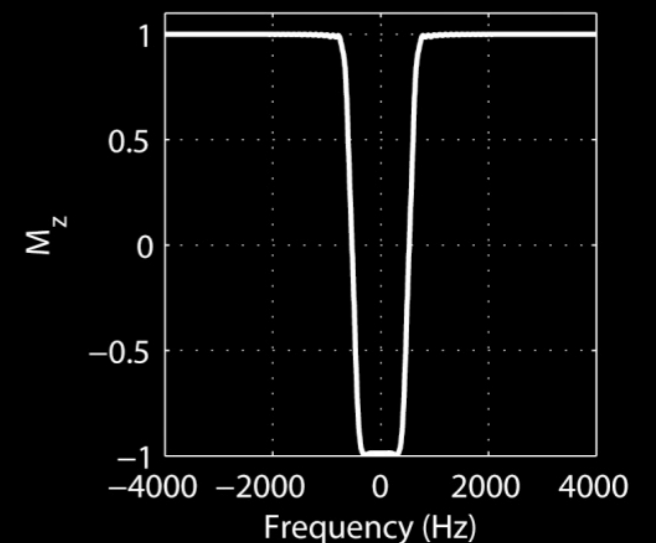
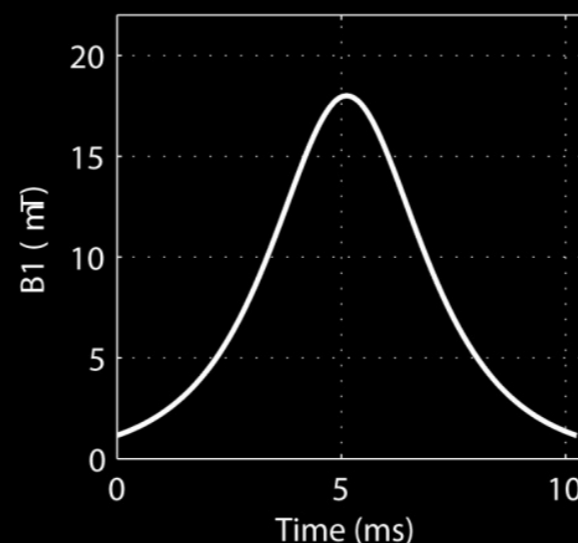
125% Amplified Pulse

$$B_1 = 15 \mu\text{T}$$



150% Amplified Pulse

$$B_1 = 18 \mu\text{T}$$



Comments

- Many envelope/modulation functions work
- If a range of adiabaticity is required, optimization can help reduce pulse length
- Hyperbolic secant needs to be truncated, which can affect the overall performance

Applications of Adiabatic Pulses

Adiabatic Pulses

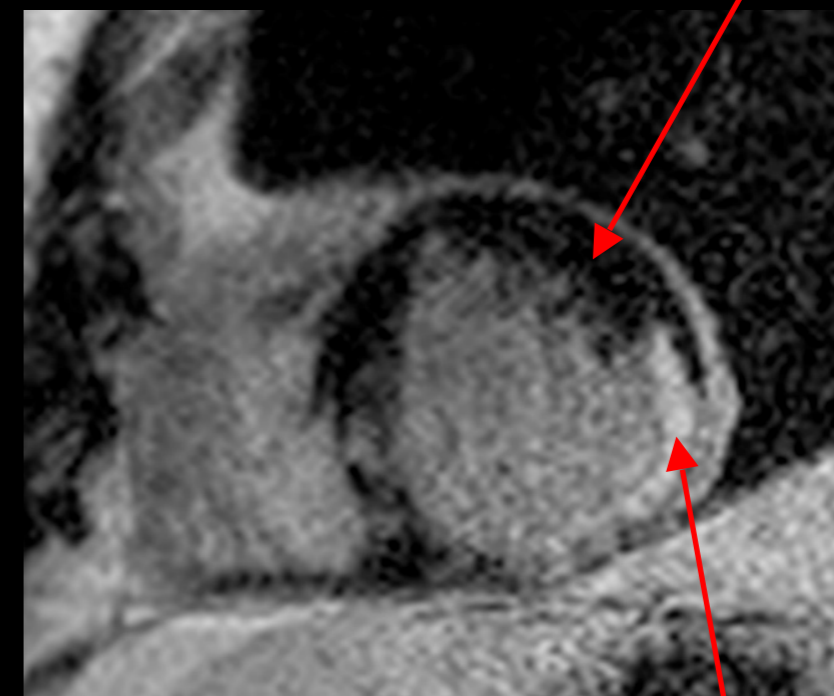
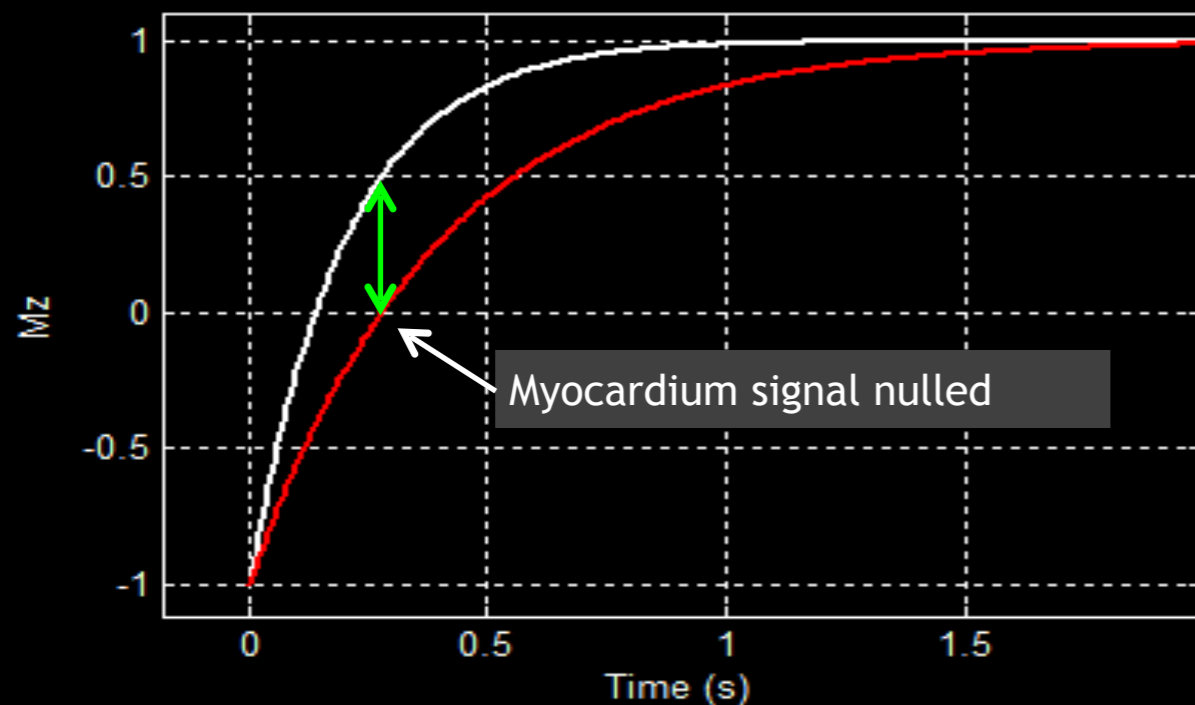
- Fat suppression (STIR)
- CSF suppression (FLAIR)
- Myocardium suppression in cardiac scar imaging (LGE)
- Black blood cardiac imaging (DIR TSE)
- T_1 Mapping

Late Gadolinium Enhancement (LGE)

- Gold standard for detection of scar/myocardial fibrosis
- Spoiled gradient echo (SPGR) sequence with an inversion pulse (inversion recovery SPGR)
 - Inversion pulse is usually hyperbolic secant pulse
 - Healthy myocardium is nulled with the inversion pulse
 - Scar tissue (which has shorter T_1 than healthy tissue) appear bright

- The conventional LGE sequence uses an RF-spoiled gradient echo (FLASH) readout with an inversion recovery (IR) pulse as a preparation pulse
- The readout is acquired at a time after inversion at which the healthy myocardium signal reaches zero

Inversion recovery curves of postcontrast scar (white) and myocardium (red)

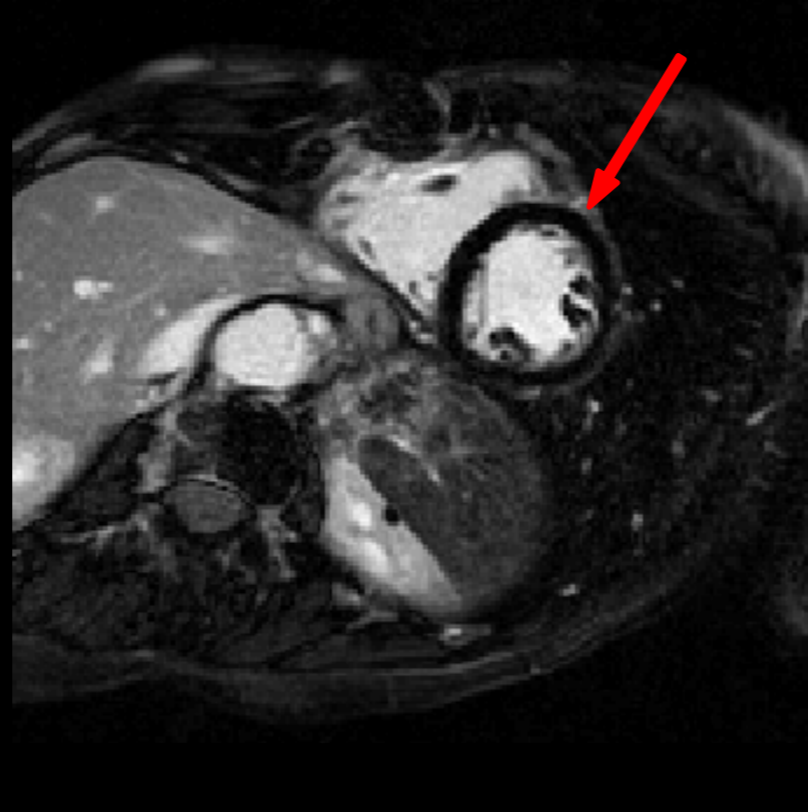


Hyper-enhanced scar region

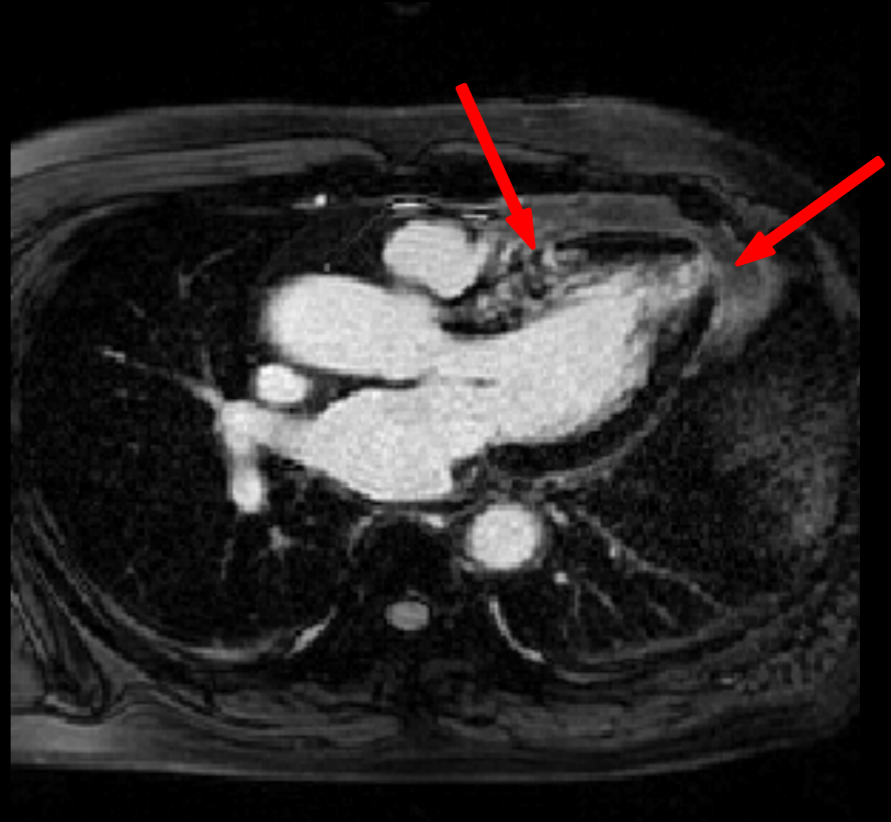
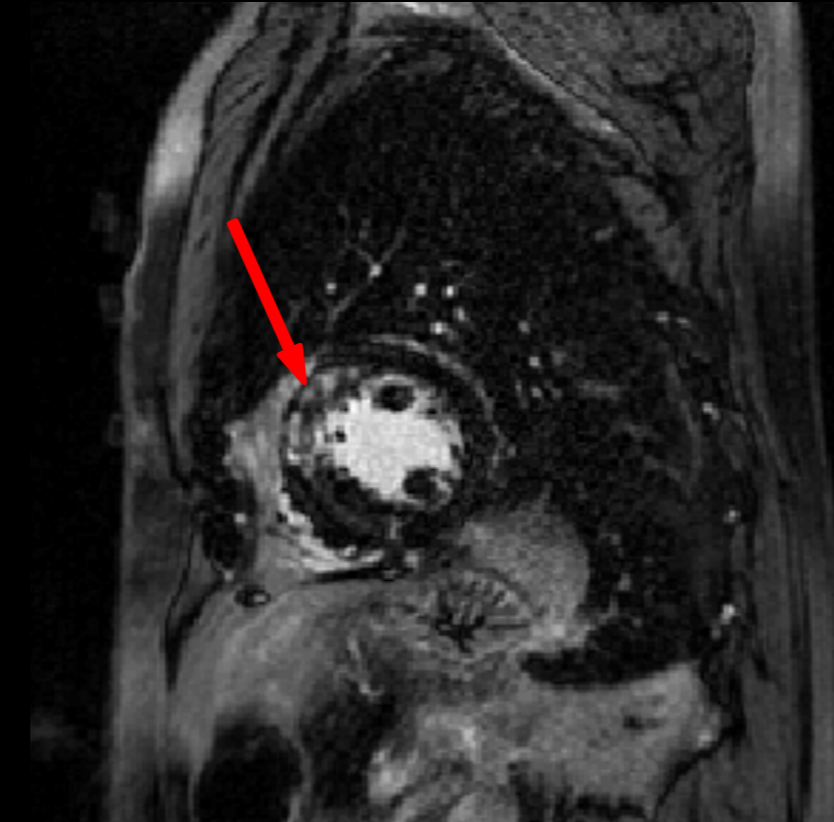
Nulled signal from healthy myocardium

Clinical Example

Patient with healthy myocardium



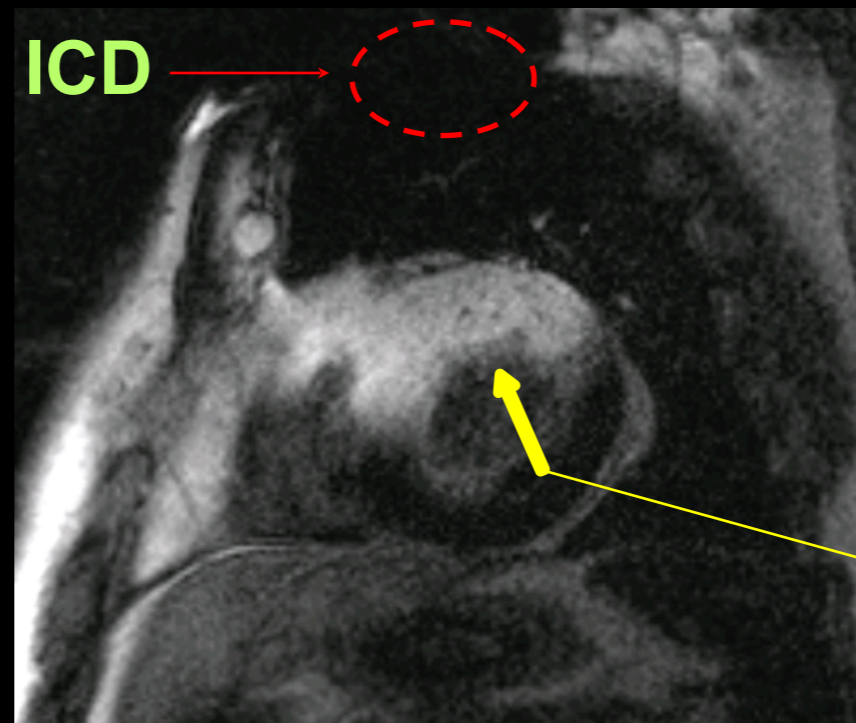
Patient with scar tissue



Clinical Example

Late Gadolinium Enhancement (LGE) in patients with implantable cardiac devices

- Presence of an implantable cardiac device in the patients produces an interesting off-resonance artifact

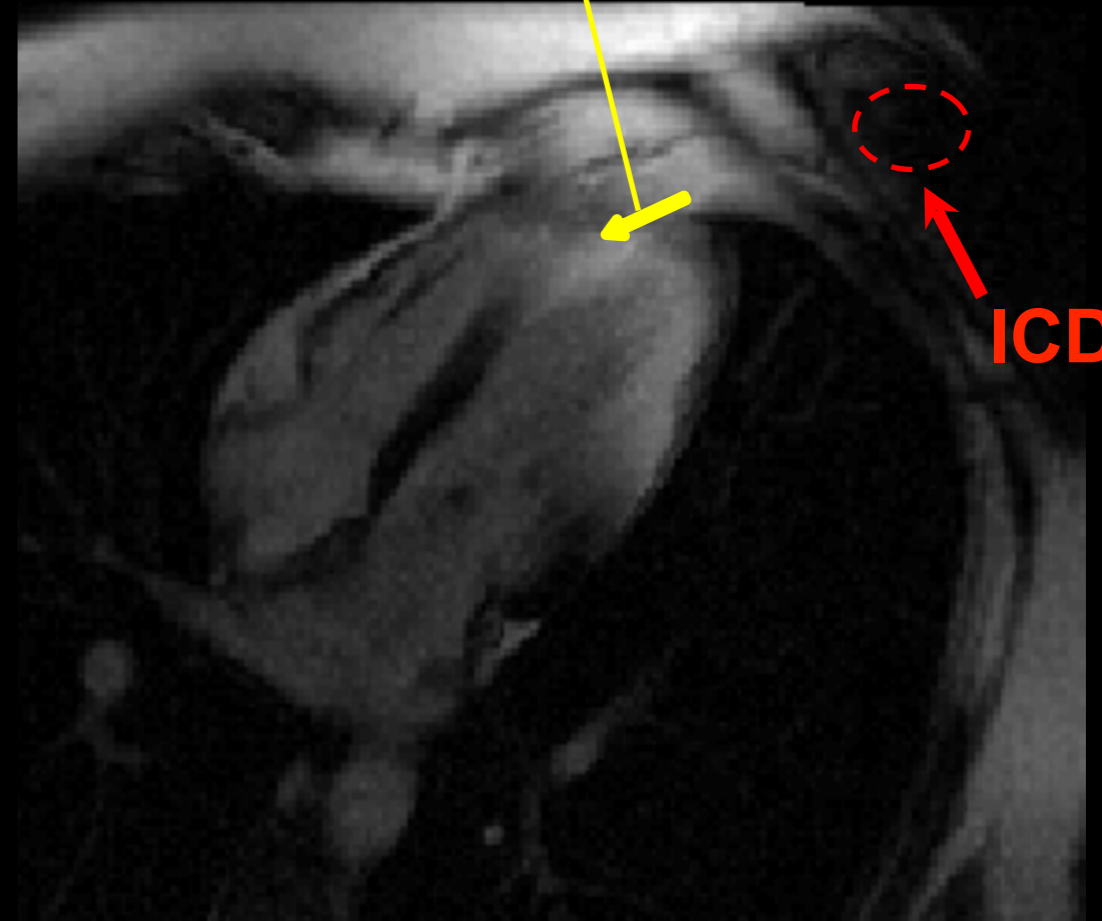


**Hyper-
intensity
Artifacts**

Hyper-intensity artifact

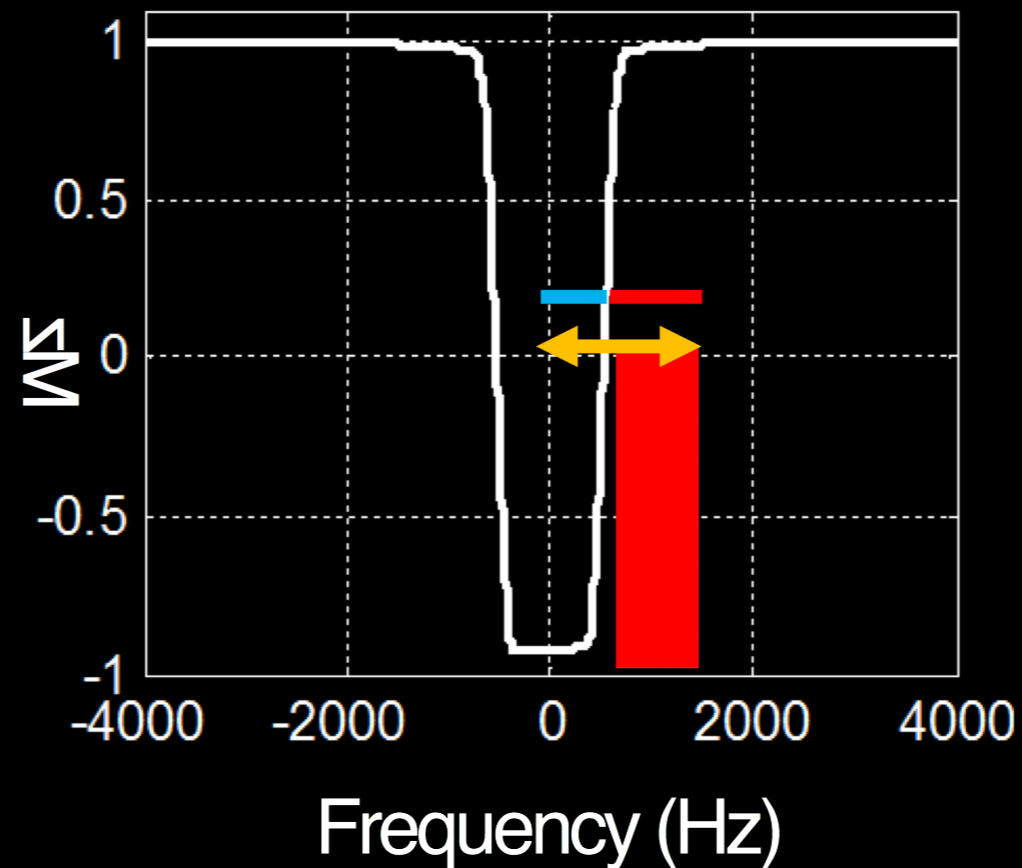


**Conventional IR
LGE Image**



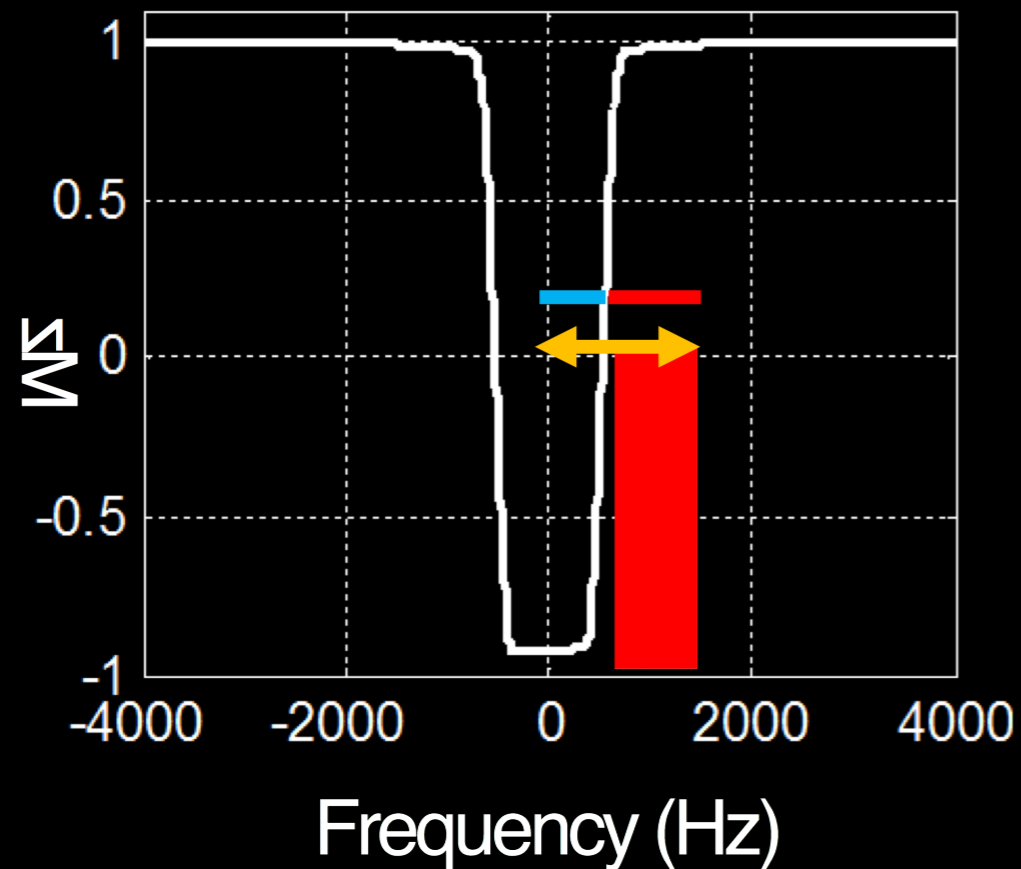
**Conventional IR
LGE Image**

Cause of Artifact

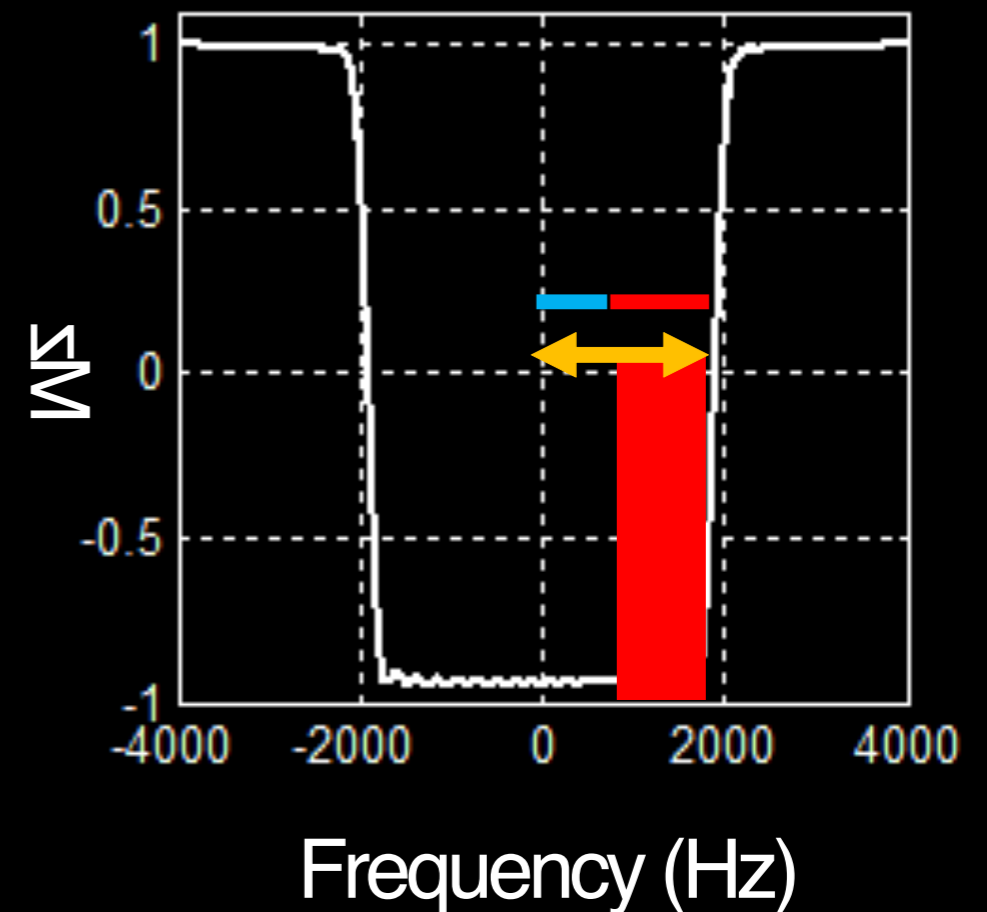


Longitudinal magnetization produced by
conventional IR pulse
BW = 1.1 kHz

Solution: Increase Bandwidth of Inversion Pulse

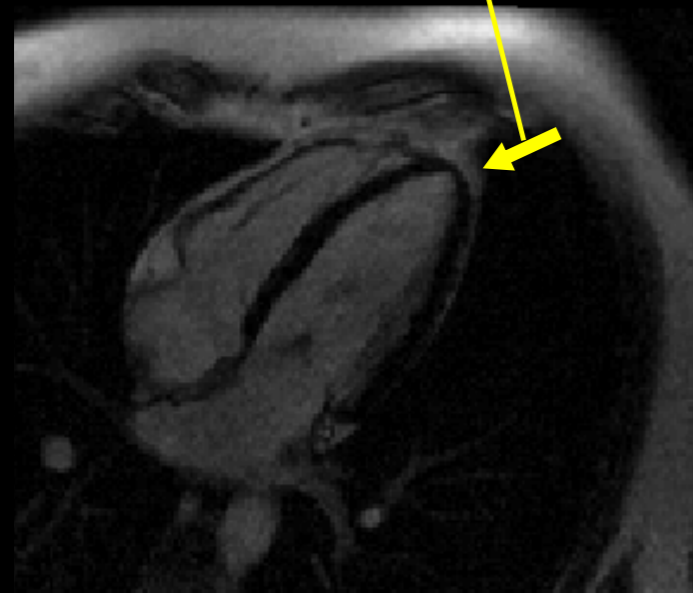


Longitudinal magnetization produced by
conventional IR pulse
BW = 1.1 kHz



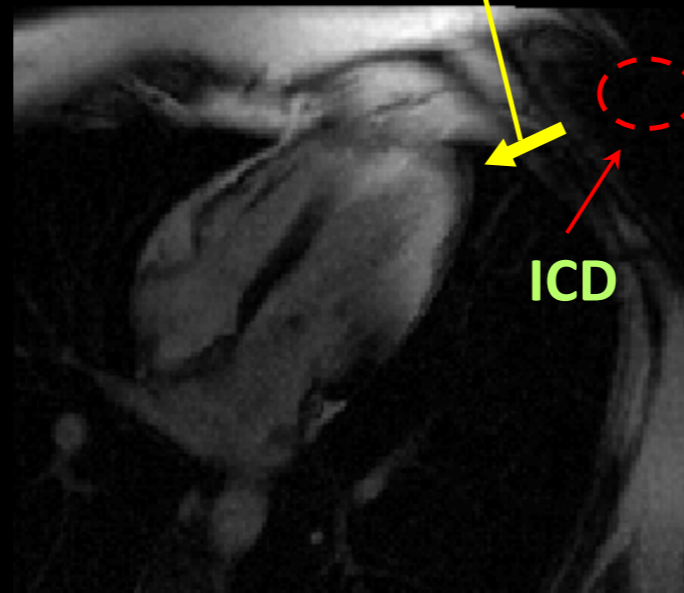
Longitudinal magnetization produced
by wideband IR pulse
BW = 3.8 kHz

No artifact (no ICD)



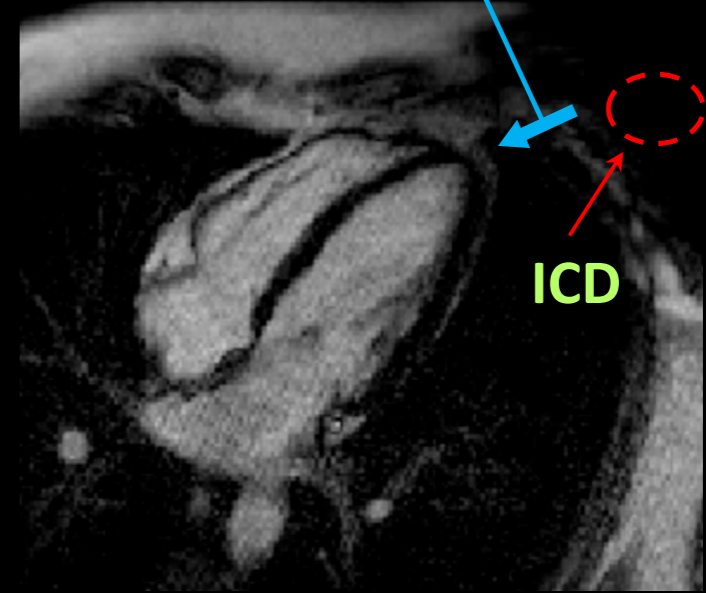
Conventional IR
LGE Image

Hyper-intensity artifact



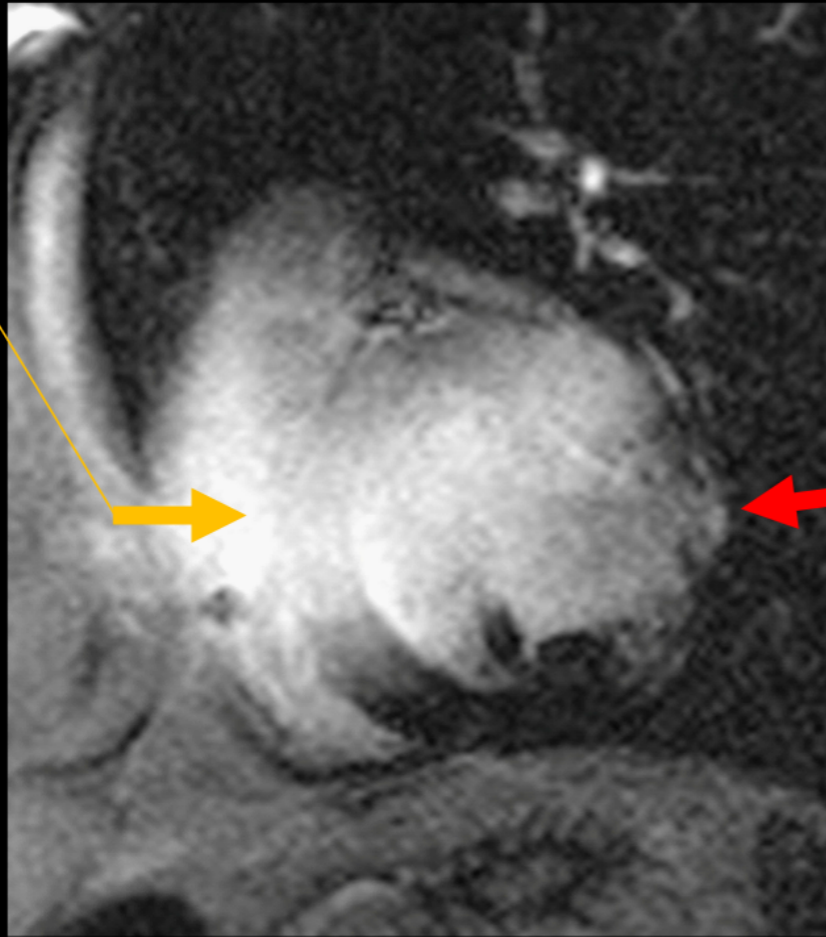
Conventional IR
LGE Image

Hyper-intensity artifact corrected



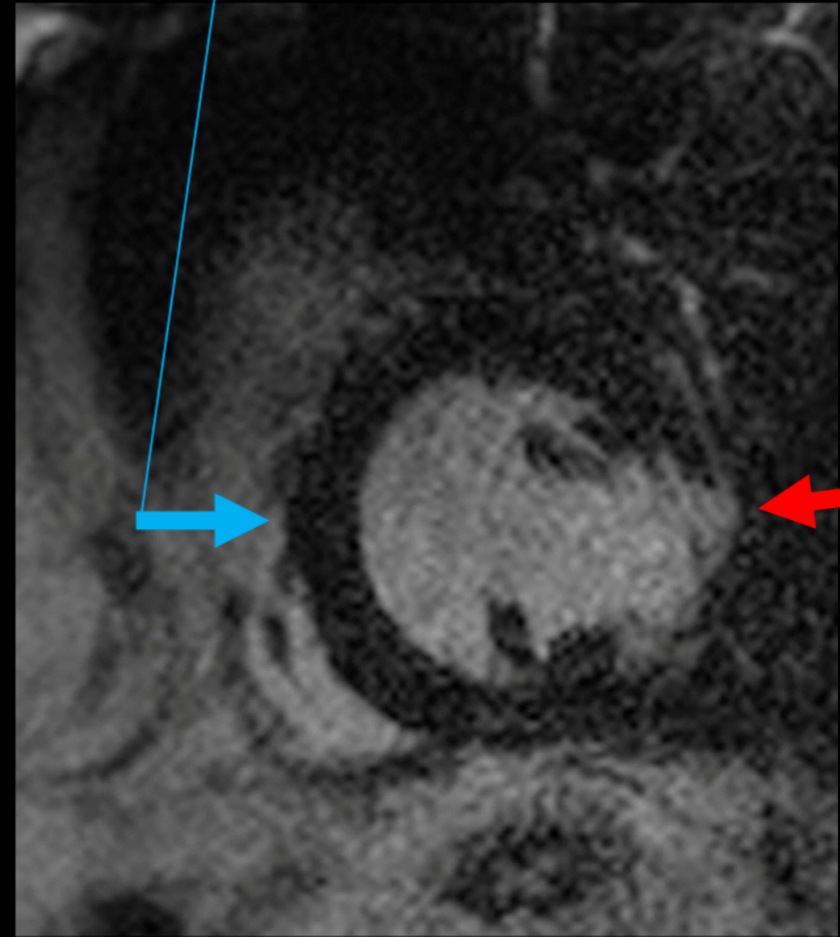
Wideband IR
LGE Image

Hyper-intensity artifacts



Antero-lateral scar
difficult to diagnose

**Artifacts
eliminated**



Antero-lateral
scar clearly
visible

MATLAB Demo

```

%%% User inputs:
mu = 5;      % Phase modulation parameter [dimensionless]
beta1 = 672; % Frequency modulation parameter [rad/s]
pulseWidth = 10.24; % RF pulse duration [ms]
A0 = 0.12;   % Peak B1 amplitude [Gauss].

%%%%%%%%

nSamples = 512; % number of samples in the RF pulse
dt = pulseWidth/nSamples/1000; % time step, [seconds]
tim_sech = linspace(-pulseWidth/2,pulseWidth/2,nSamples)./1000';
% time scale to calculate the RF waveforms in seconds.

% Amplitude modulation function B1(t):
B1 = A0.* sech(beta1.*tim_sech);

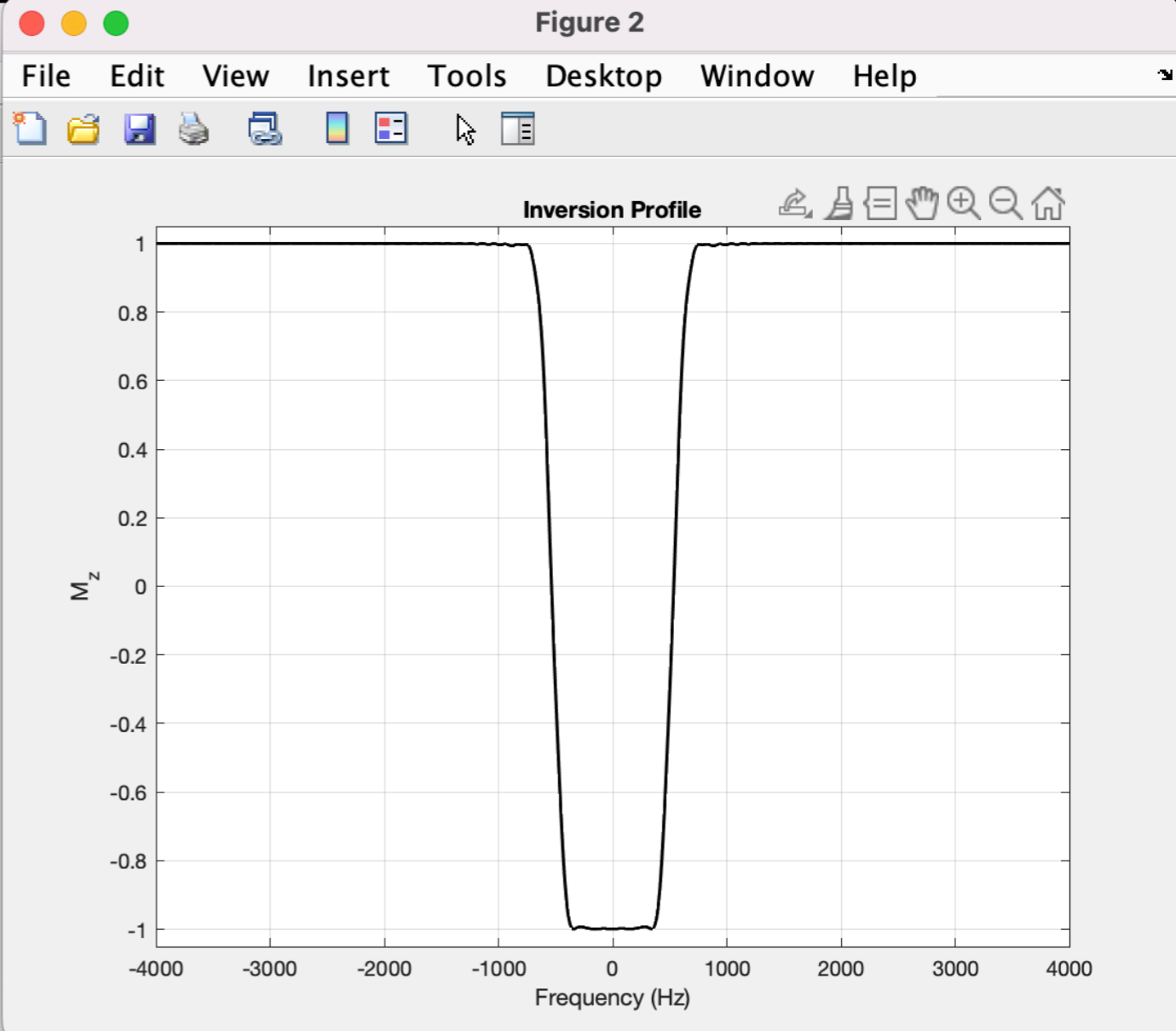
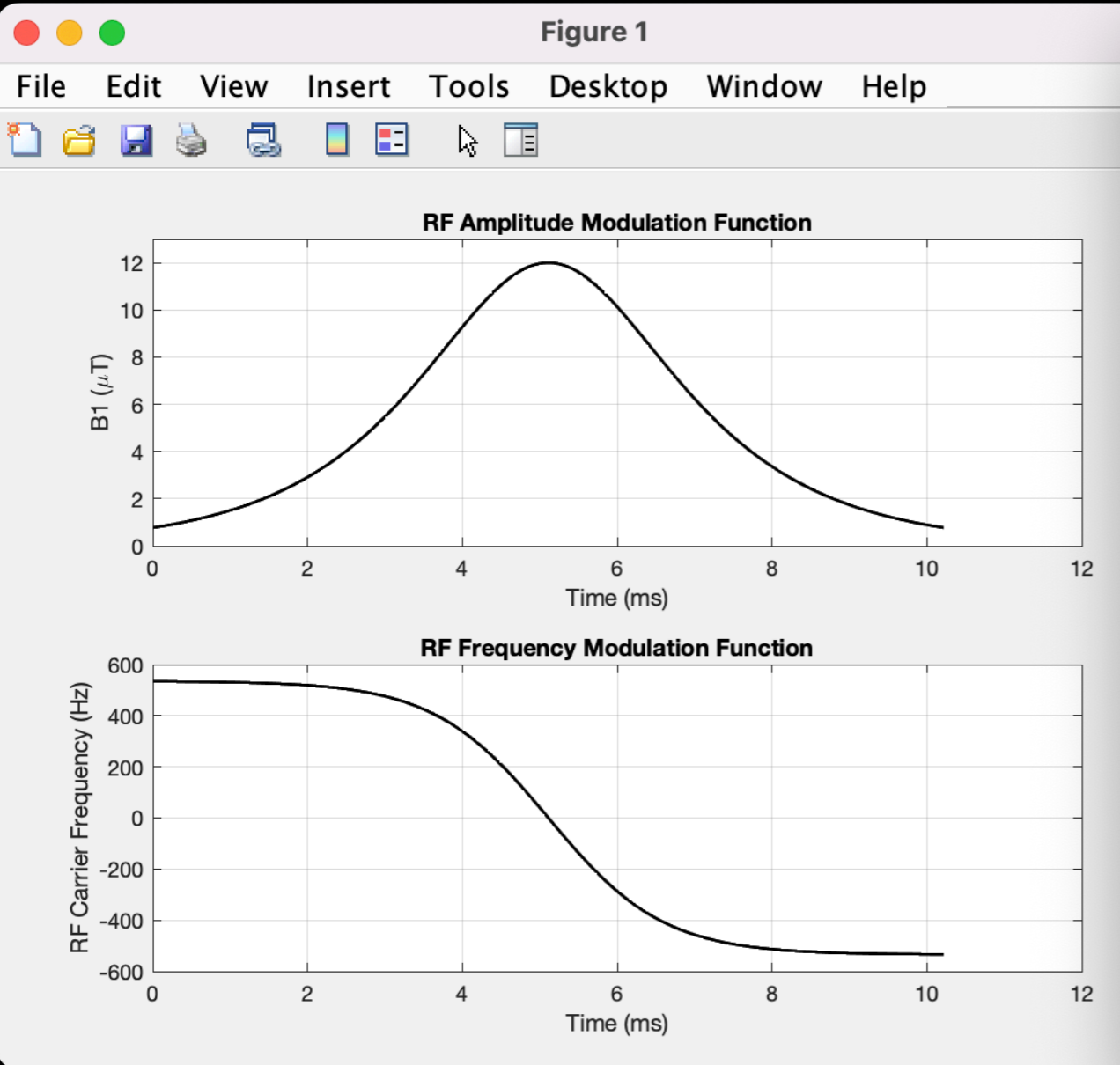
% Carrier frequency modulation function w(t):
w = -mu.*beta1.*tanh(beta1.*tim_sech)./(2*pi);
% The 2*PI scaling factor at the end converts the unit from rad/s to Hz

% Phase modulation function phi(t):
phi = mu .* log(sech(beta1.*tim_sech));

% Put together complex RF pulse waveform:
rf_pulse = B1 .* exp(1i.*phi);

% Generate a time scale for the Bloch simulation:
tim_bloch = [0:(nSamples-1)]*dt;

```



Thank You!

- Further reading

- Read "Adiabatic Refocusing Pulses" p.200-212
- Tannus et al., "Adiabatic Pulses", NMR in Biomedicine, Vol. 10, 423-434 (1997)

- Acknowledgments

- John Pauly's EE469B (RF Pulse Design for MRI)
- Shams Rashid
- Kyung Sung

Holden H. Wu, PhD

HoldenWu@mednet.ucla.edu

<https://mrrl.ucla.edu/wulab>