Spatial Localization II

M219 - Principles and Applications of MRI
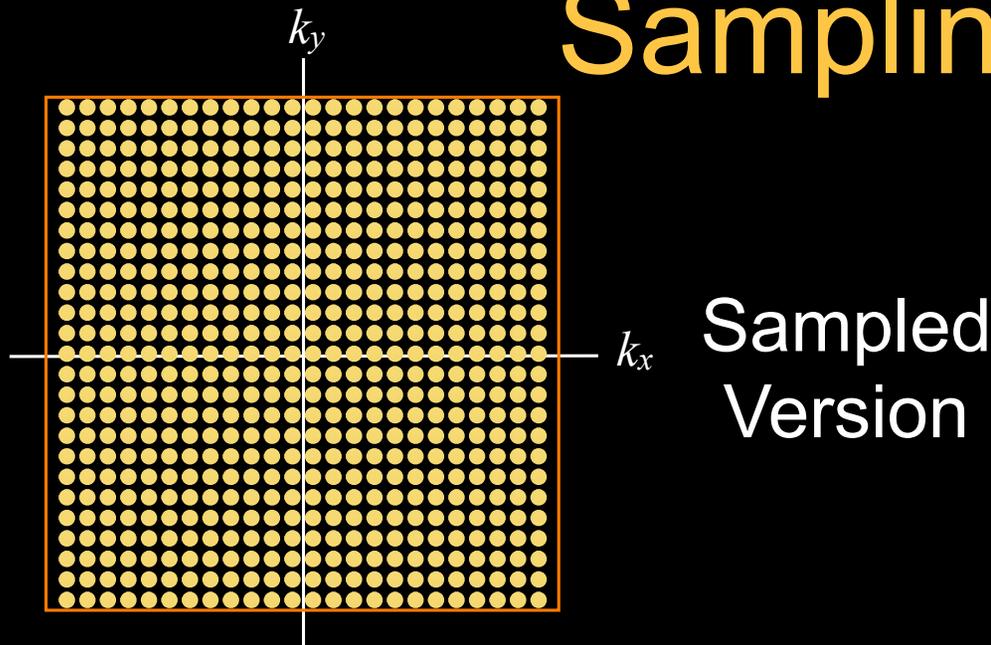### Kyung Sung, Ph.D.
2/8/2023

Course Overview

- 2023 course schedule
  - https://mrrl.ucla.edu/pages/m219_2023

- Assignments
  - Homework #2 is due on 2/15

- Office hours, Fridays 10-12pm
  - In-person (Ueberroth, 1417B)
  - Zoom is also available (https://uclahs.zoom.us/j/98066349714?pwd=cnVmV1J5QjR1d3I3cmJkQnVLSFZVZz09)

Spatial Resolution

Sampling Model

k_y

k_x

Sampled Version

$$\hat{M}(k_x, k_y) = M(k_x, k_y) \cdot \underbrace{\text{III}(\frac{k_x}{\Delta k_x}, \frac{k_y}{\Delta k_y})\frac{1}{\Delta k_x \Delta k_y}}_{\text{Sampling}} \underbrace{\sqcap(\frac{k_x}{w_{k_x}}, \frac{k_y}{w_{k_y}})}_{\text{Extent}}$$

FT $\updownarrow$

$$\hat{m}(x, y) = m(x, y) * \underbrace{\text{III}(\Delta k_x x, \Delta k_y y)}_{\text{Field of View}} * \underbrace{sinc(w_{k_x} x)sinc(w_{k_y} y)}_{\text{Spatial Resolution}}$$

Point Spread Function (PSF)

$$\hat{M}(k_x, k_y) = M(k_x, k_y) \cdot \mathrm{III}(\frac{k_x}{\Delta k_x}, \frac{k_y}{\Delta k_y}) \frac{1}{\Delta k_x \Delta k_y} \underset{\text{Extent}}{\sqcap (\frac{k_x}{w_{k_x}}, \frac{k_y}{w_{k_y}})}$$
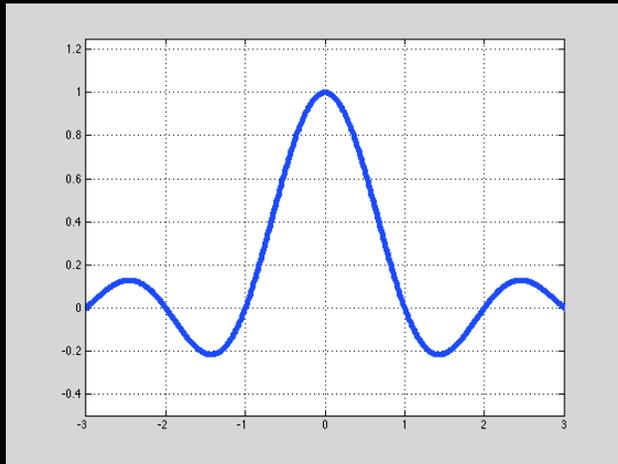
$$\hat{M}'(k_x, k_y) = \hat{M}(k_x, k_y) \cdot \mathrm{window}$$

$$\mathrm{PSF} = \mathrm{FT}(\mathrm{window})$$

Point spread function can show
the extent of blurring of the image

Spatial Resolution

$$m(x, y) * sinc(w_{k_x} x) sinc(w_{k_y} y) w_{k_x} w_{k_y}$$

Main lobe causes blurring!
(spatial resolution)

Spatial resolution: δ_x, δ_y

$$\delta_x = \frac{1}{w_{k_x}} \qquad \delta_y = \frac{1}{w_{k_y}}$$
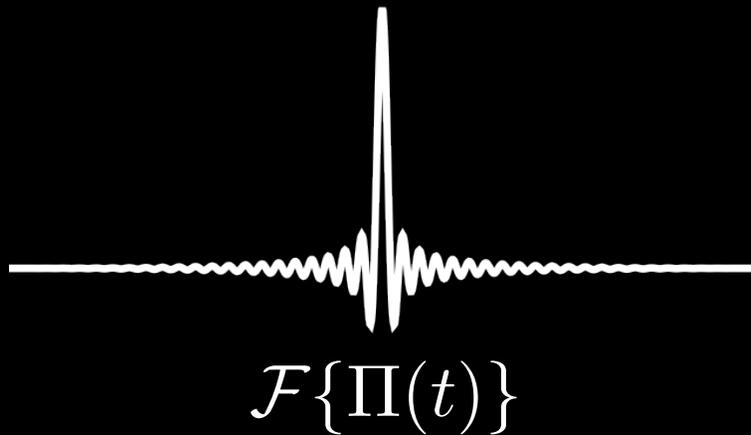
To the Board

Spatial Resolution

- Spatial resolution of an imaging system is the smallest separation δx of two point sources necessary for them to remain resolvable in the resultant image.
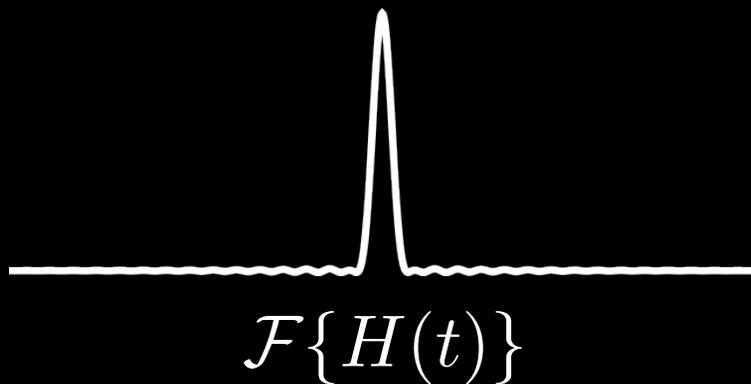
$$\hat{I}(x) = I(x) * h(x)$$

Image   Object   Point Spread Function

PSFs

$\mathcal{F}\{\Pi(t)\}$

Narrower central peak, but lots of ringing

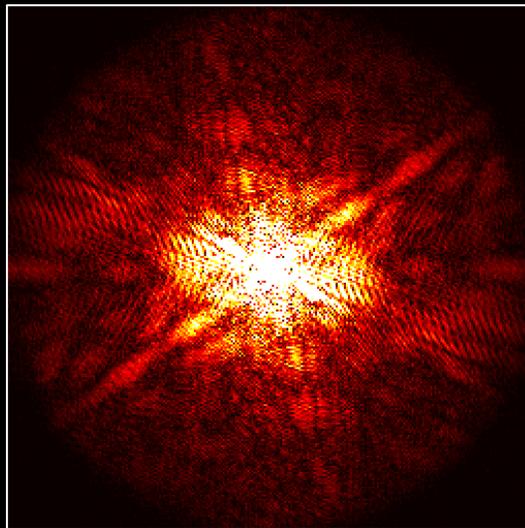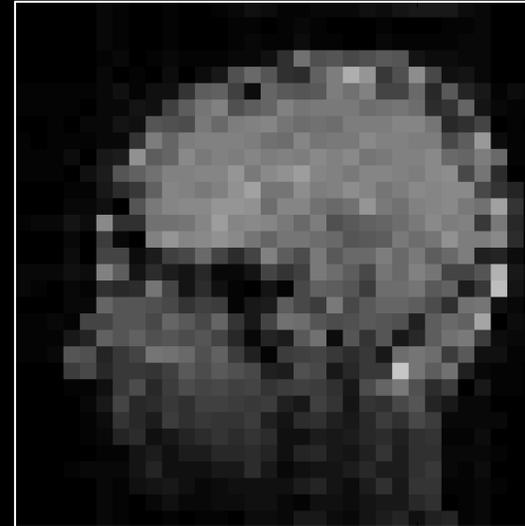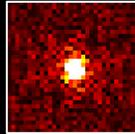$\mathcal{F}\{H(t)\}$

Reduced ringing, but broader central peak

PSFs

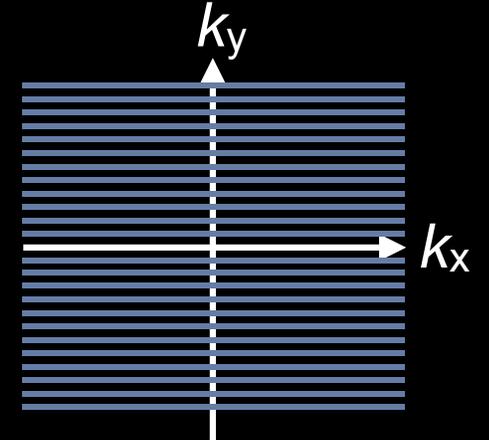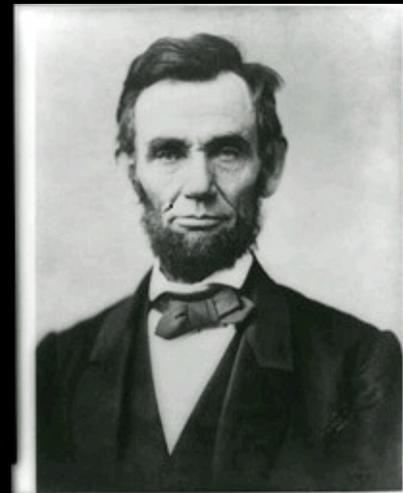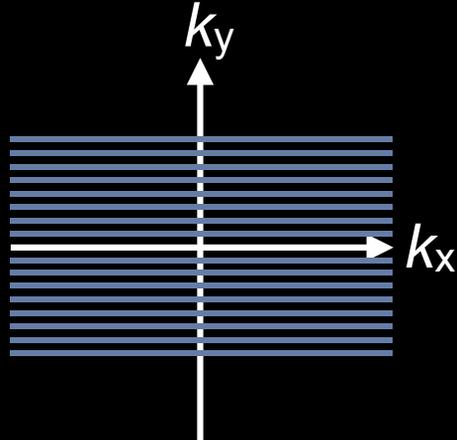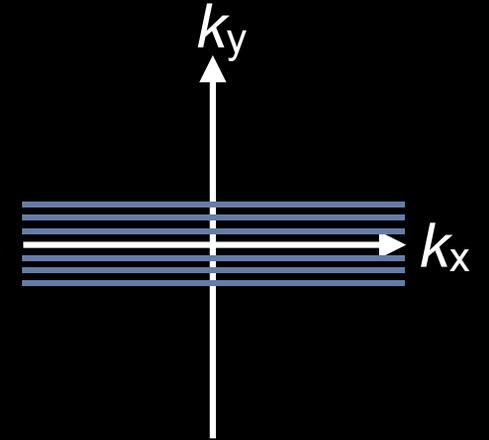Filters can be used to reduce ringing artifacts but often at the expense of spatial resolution

Hamming window seems to have good balance in reducing ringing

Finite Sampling

$$W_h = \frac{1}{N\Delta k} = \frac{FOV}{N}$$

k-space Sampling

example from Dan
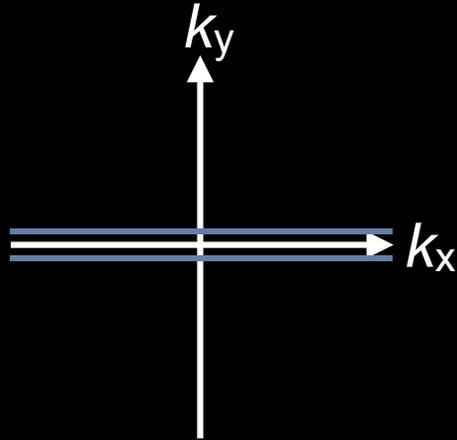
k-space Sampling

k-space Sampling

example from Dan
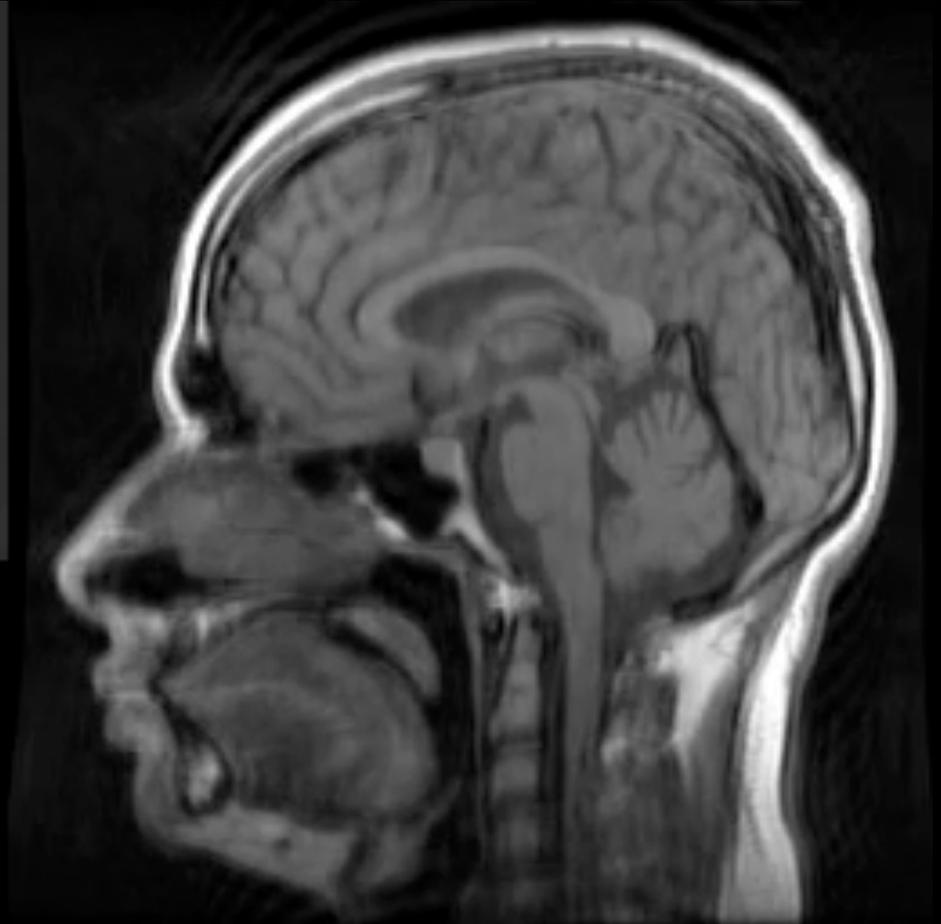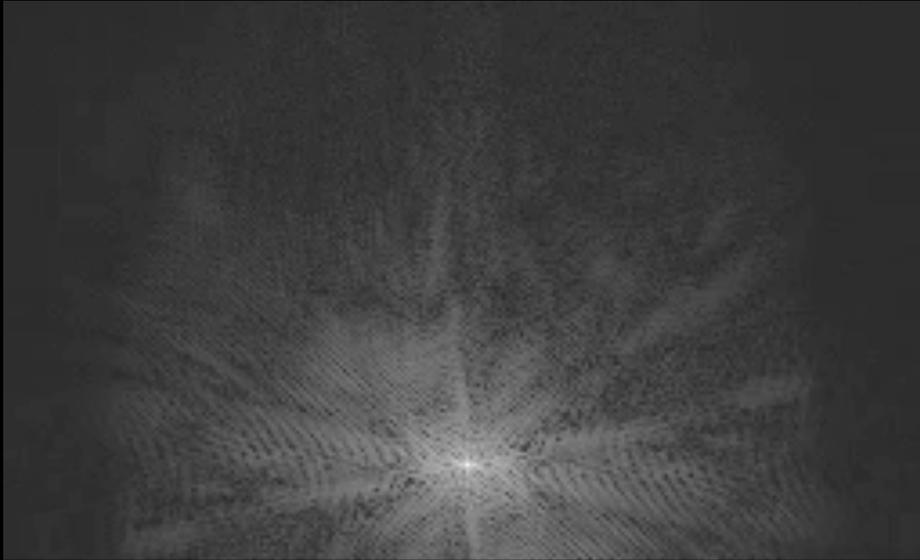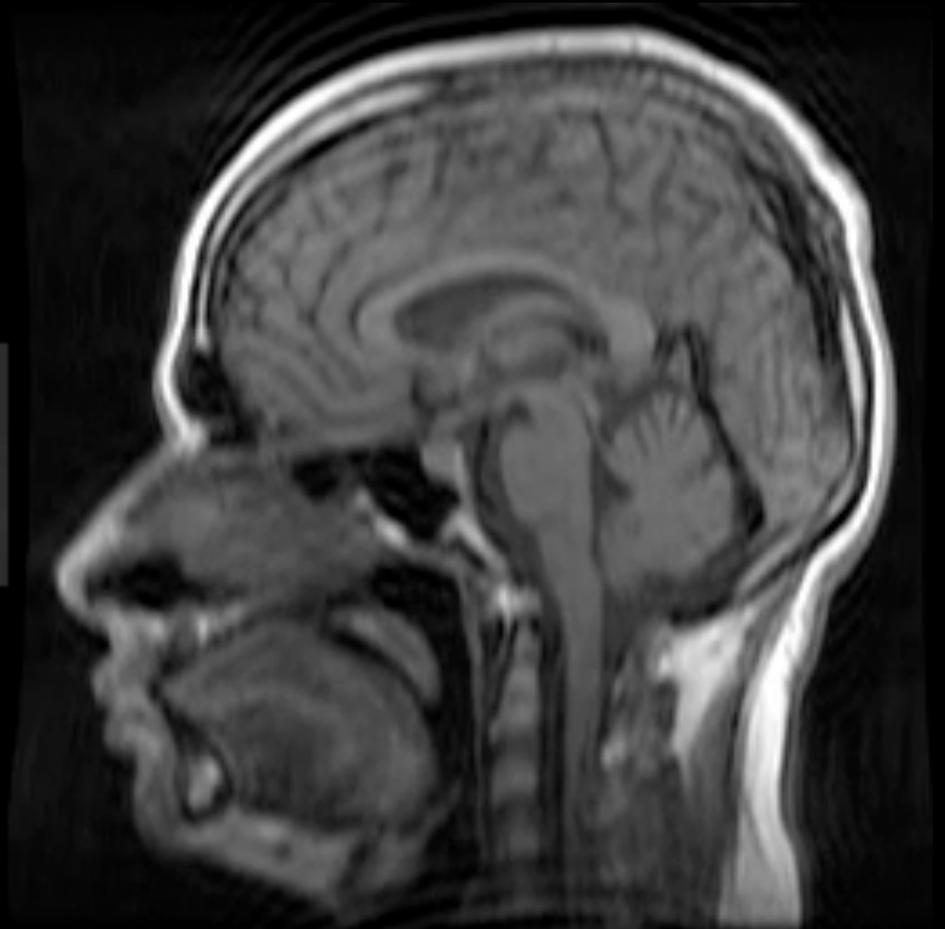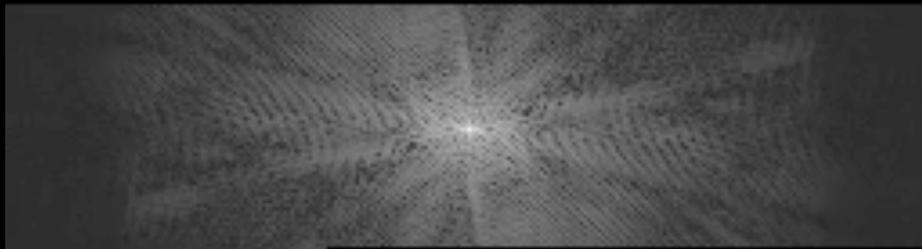
Gibb's Ringing

Distortions in the profile arising
from the finite sampling of the data

$$\rho_{true}(\omega) \qquad * \qquad \text{sinc}(\omega) \qquad = \qquad \rho_{meas}(\omega)$$
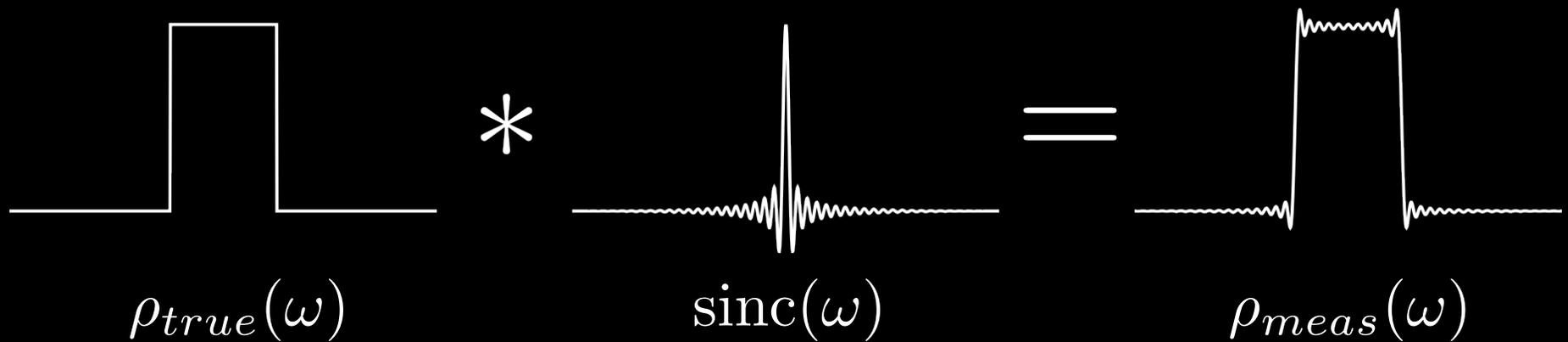
This type of distortion is most commonly
referred to as Gibb's ringing

Examples of Gibb's Ringing
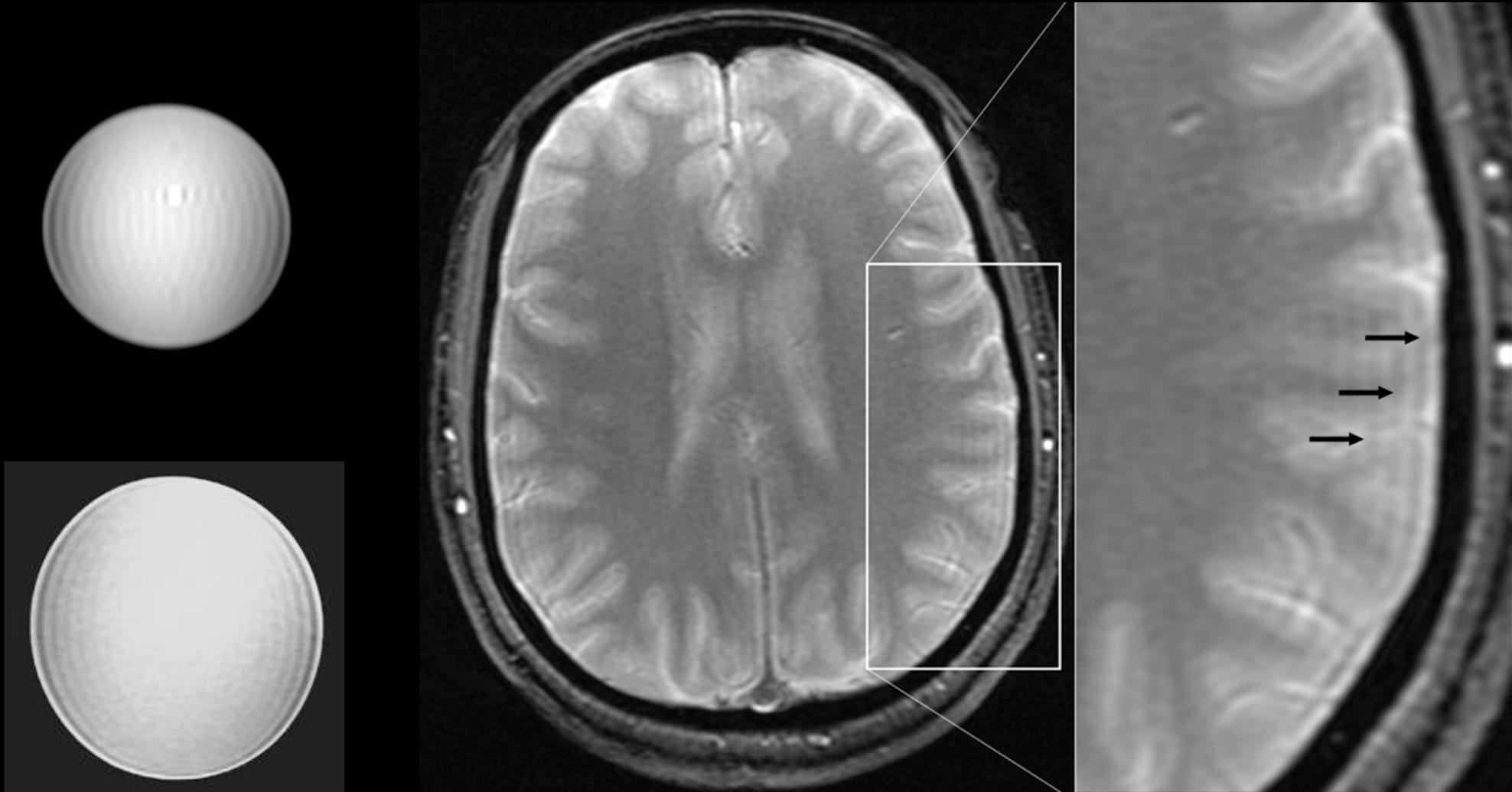
Gibb's Ringing

how to reduce ringing

$$\mathcal{F}^{-1}\{\Pi(t)\}$$

$$\mathcal{F}^{-1}\{H(t)\}$$
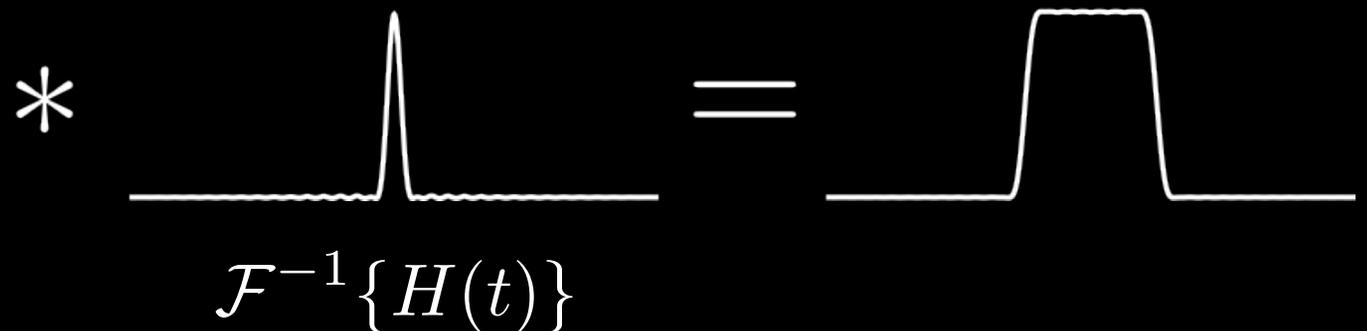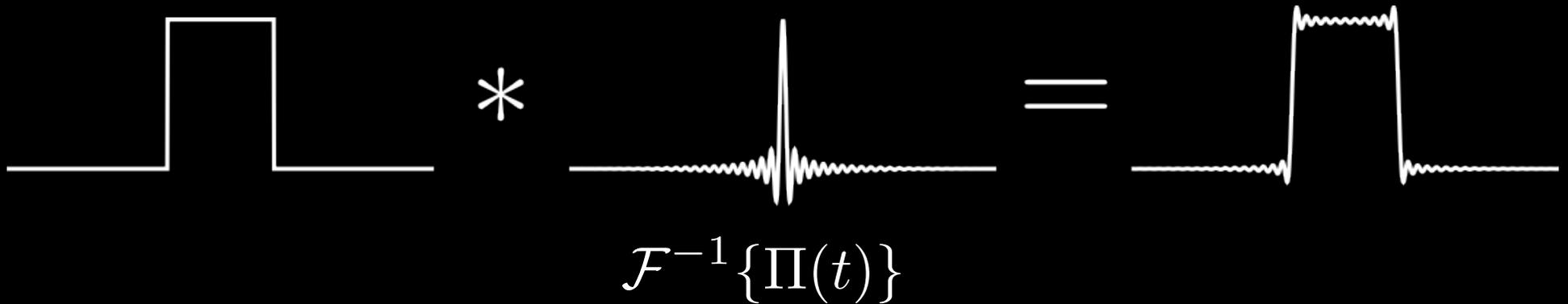
Hamming window can be used to reduce ringing

Spatial Localization

Spatial Encoding

- **Three key steps:**
  - **Slice selection**
    - You have to pick slice!
  - **Phase Encoding**
    - You have to encode 1 of 2 dimensions within the slice.
  - **Frequency Encoding** (aka *readout*)
    - You have to encode the other dimension within the slice.

3 Steps for Spatial Localization
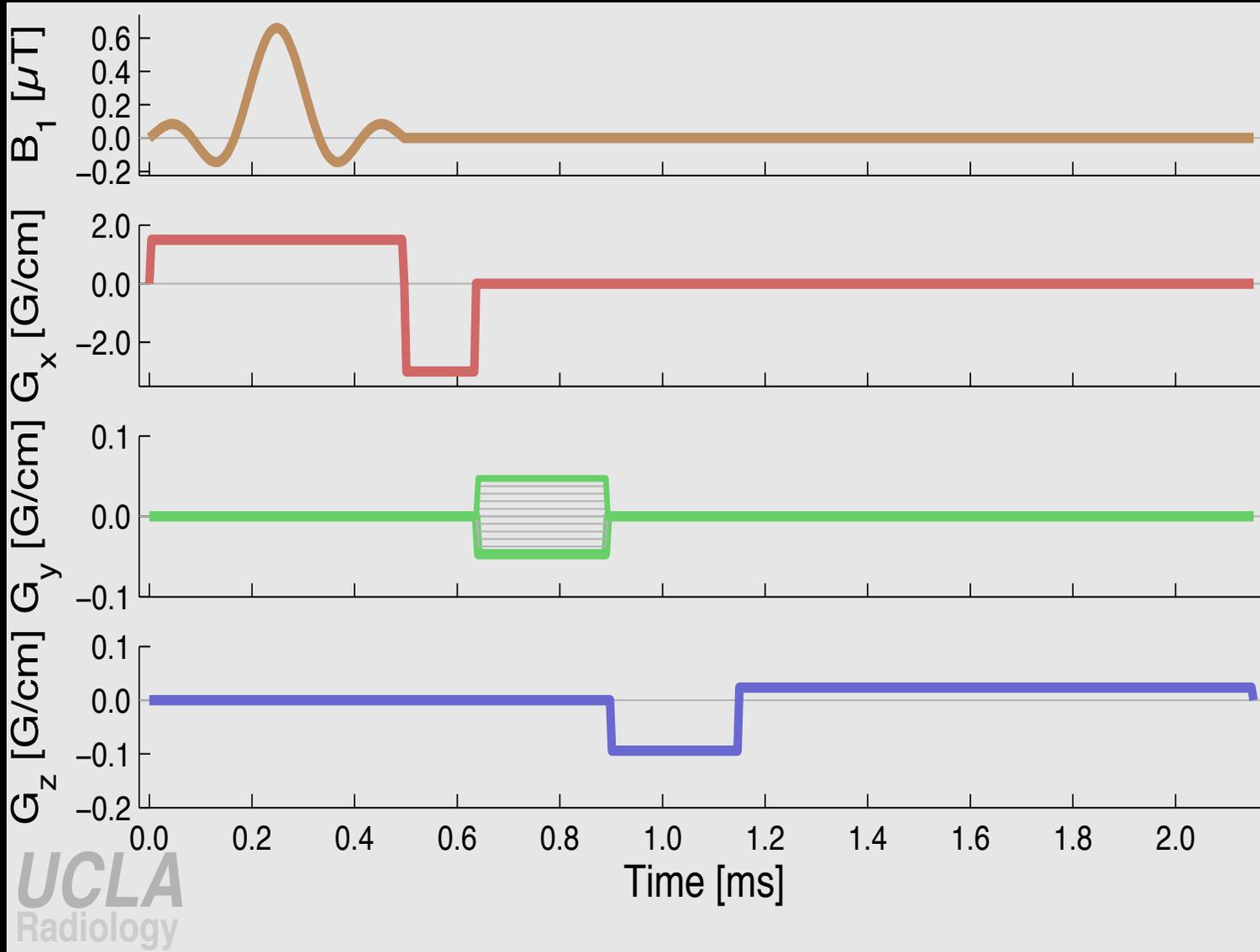
Pulse Sequence Diagram - Timing diagram of the RF and gradient events that comprise an MRI pulse sequence.

Slice Selection

- **Consists of:**
  - **RF (B_1) Pulse**
    - **Contains frequencies matched to slice of interest**
  - **Slice selection gradient**
    - **Constant magnitude**
  - **Slice re-phasing gradient**
    - **Increases SNR**
    - **Re-phases spins within slice**
    - **AKA "slice refocusing gradient"**
- **Permits exciting the slice of interest**

Selective Excitation

RF

Gz

} excite a slice perpendicular to z

x-slice
(yz plane)

y-slice
(xz plane)

z-slice
(xy plane)
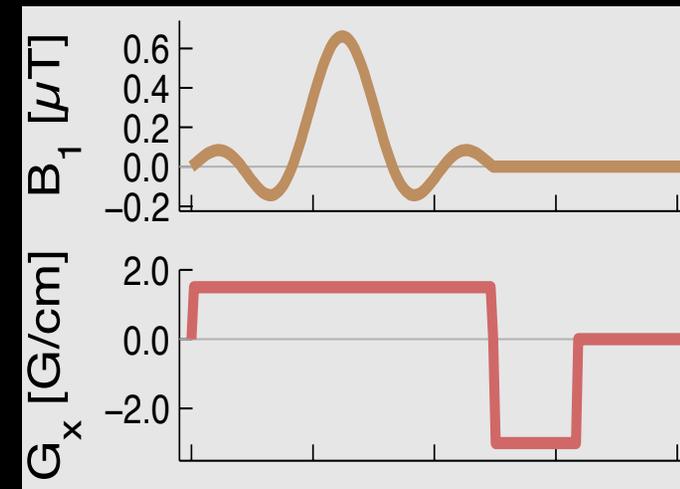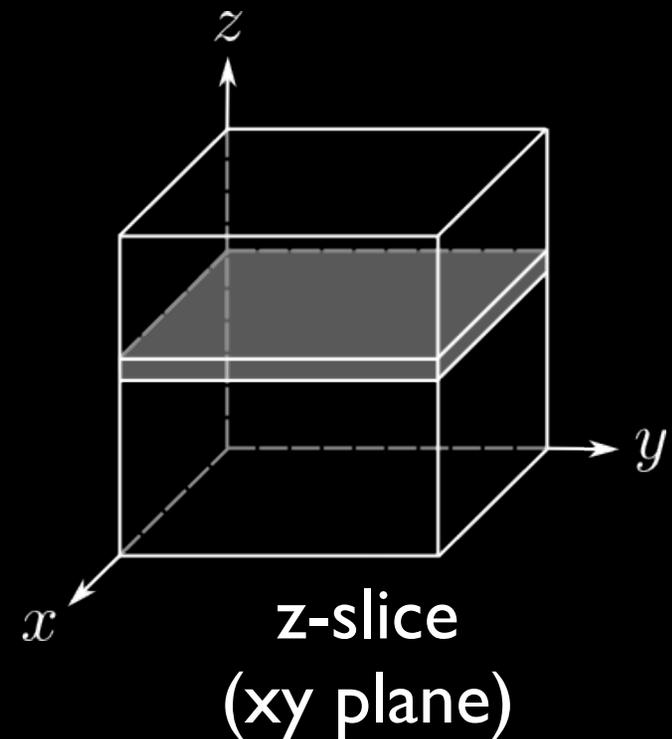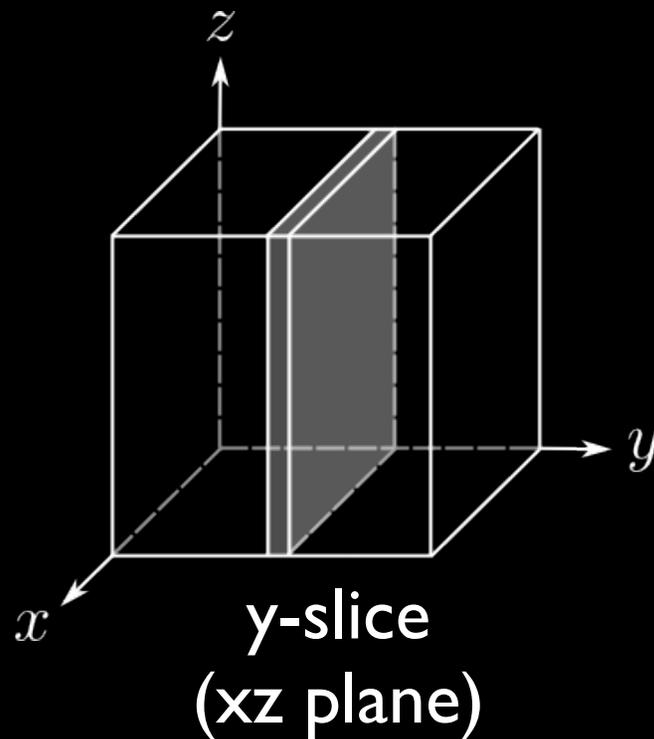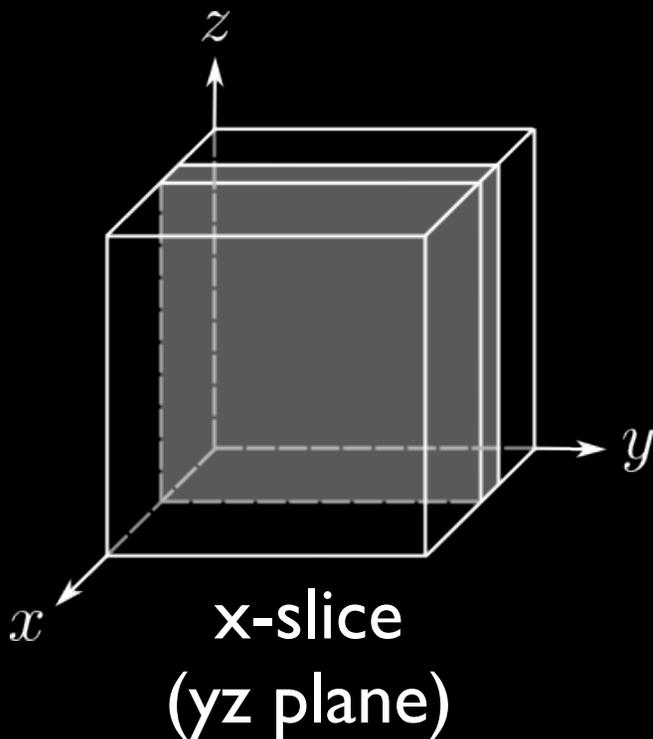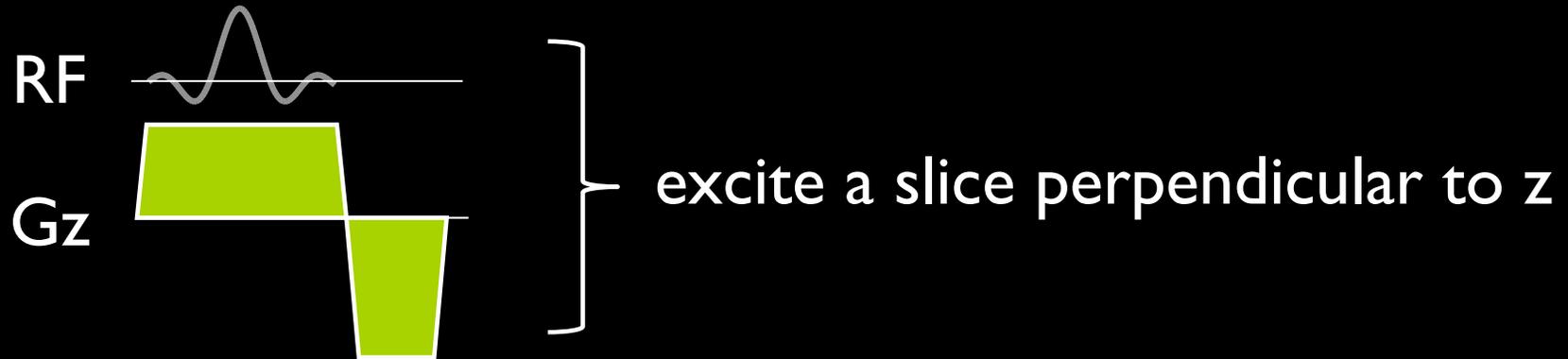
Gradients?

gradients produce a spatial distribution of frequencies

$$B_z(z) = B_0 + G_z \cdot z$$
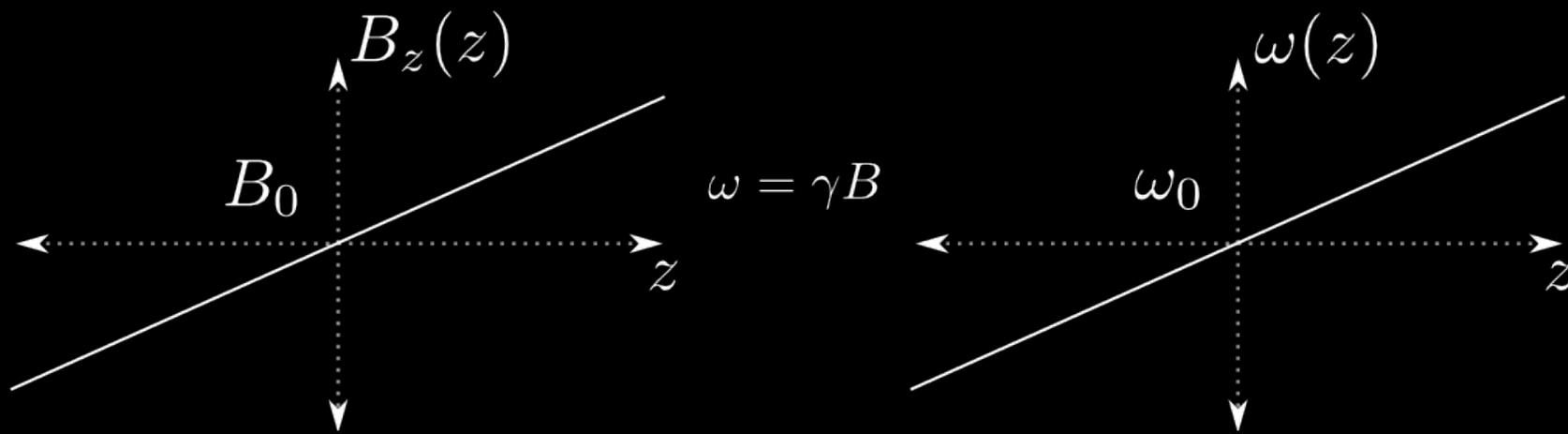
$$\omega(z) = \omega_0 + \gamma G_z \cdot z$$

there is a direct correspondence between
frequency and spatial position

Bloch Equation with Gradient

$$\frac{d\vec{M}_{rot}}{dt} = \vec{M}_{rot} \times \gamma \vec{B}_{eff}$$

$$\vec{B}_{eff} = \begin{pmatrix} B_1(t) \\ 0 \\ B_0 - \frac{\omega_{RF}}{\gamma} \end{pmatrix} \longrightarrow \vec{B}_{eff} = \begin{pmatrix} B_1(t) \\ 0 \\ B_0 - \frac{\omega_{RF}}{\gamma} + G_z z \end{pmatrix}$$

Slice Selection

how do we "excite" a certain slice?
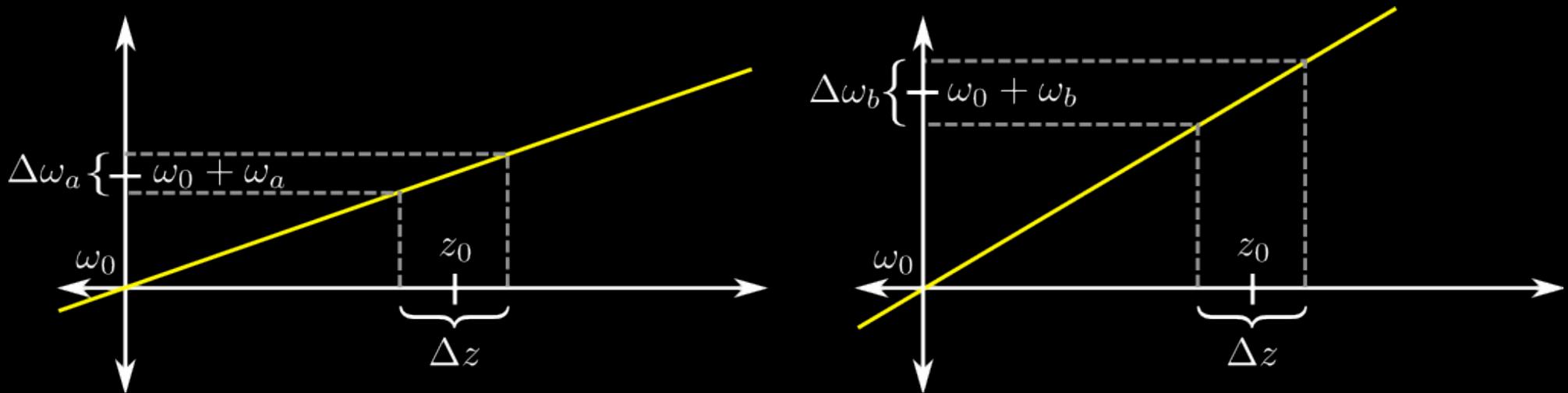
the strength of the gradient affects all
parameters for the same spatial location

$$\Delta\omega_a < \Delta\omega_b$$

$$\omega_a < \omega_b$$

Slice Selection

how do we physically set the parameters?
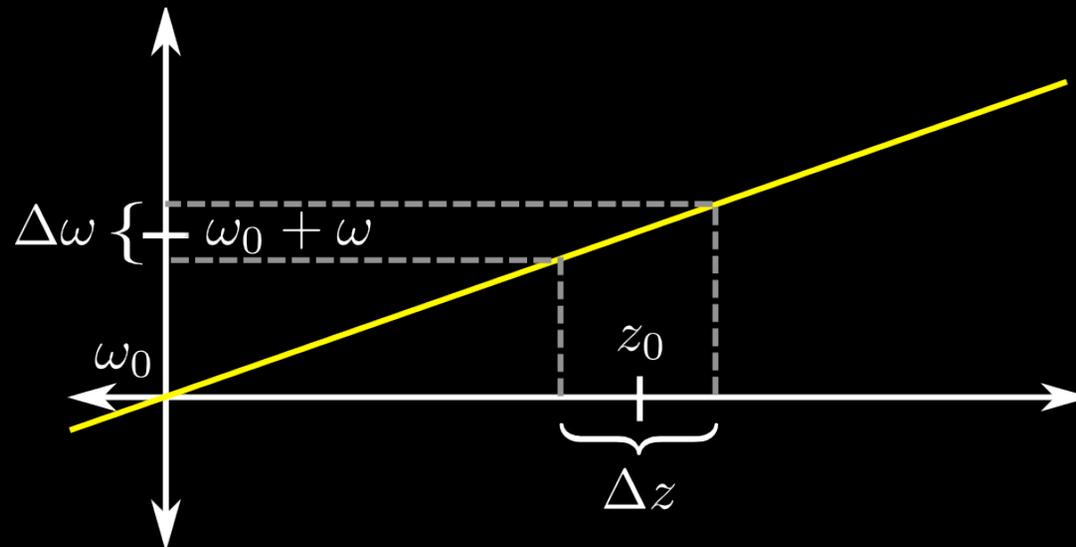
ω - the carrier frequency of the RF pulse

$\Delta\omega$ - frequency bandwidth of the RF pulse

Slice Selection
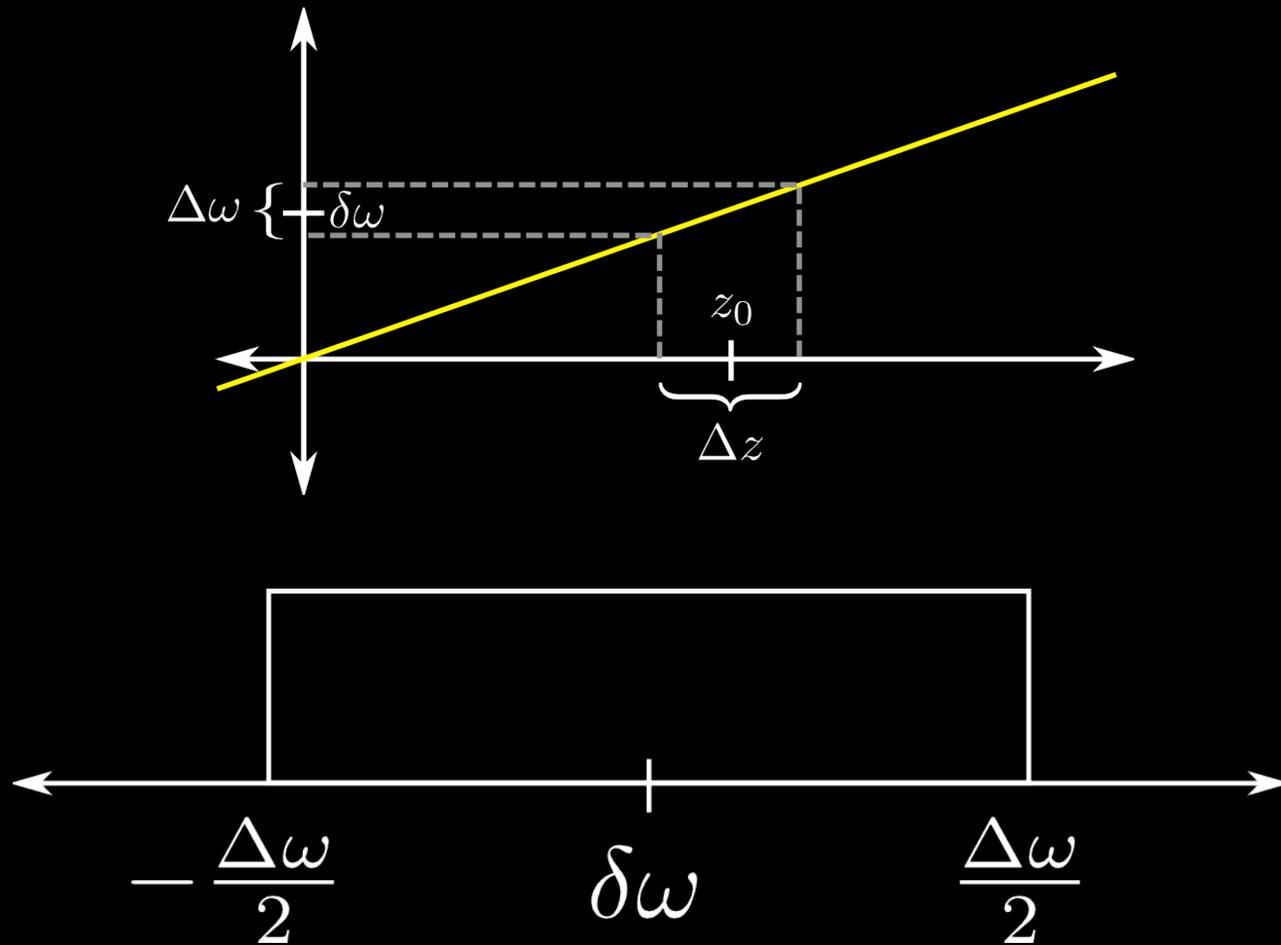
we want a pulse with as rectangular of an slice profile as possible

Selective Excitation

changing the shape of the pulse affects
the bandwidth of excitation

how we do know which shape to use?

small angle approximation

We will show the slice profile depends on

FT

z
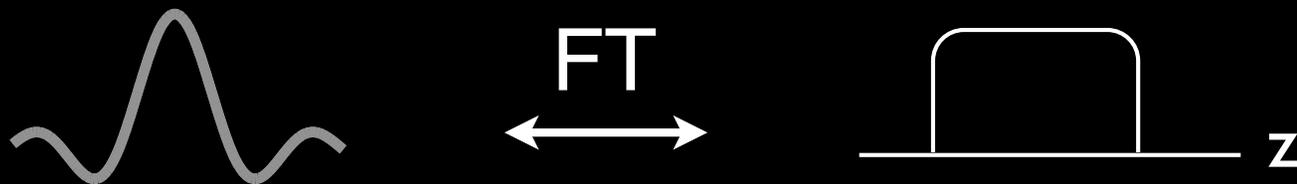
Slice Selective Excitation

$$\Delta\omega = -\gamma\left(G_z \cdot \Delta z\right)$$

Excitation Bandwidth
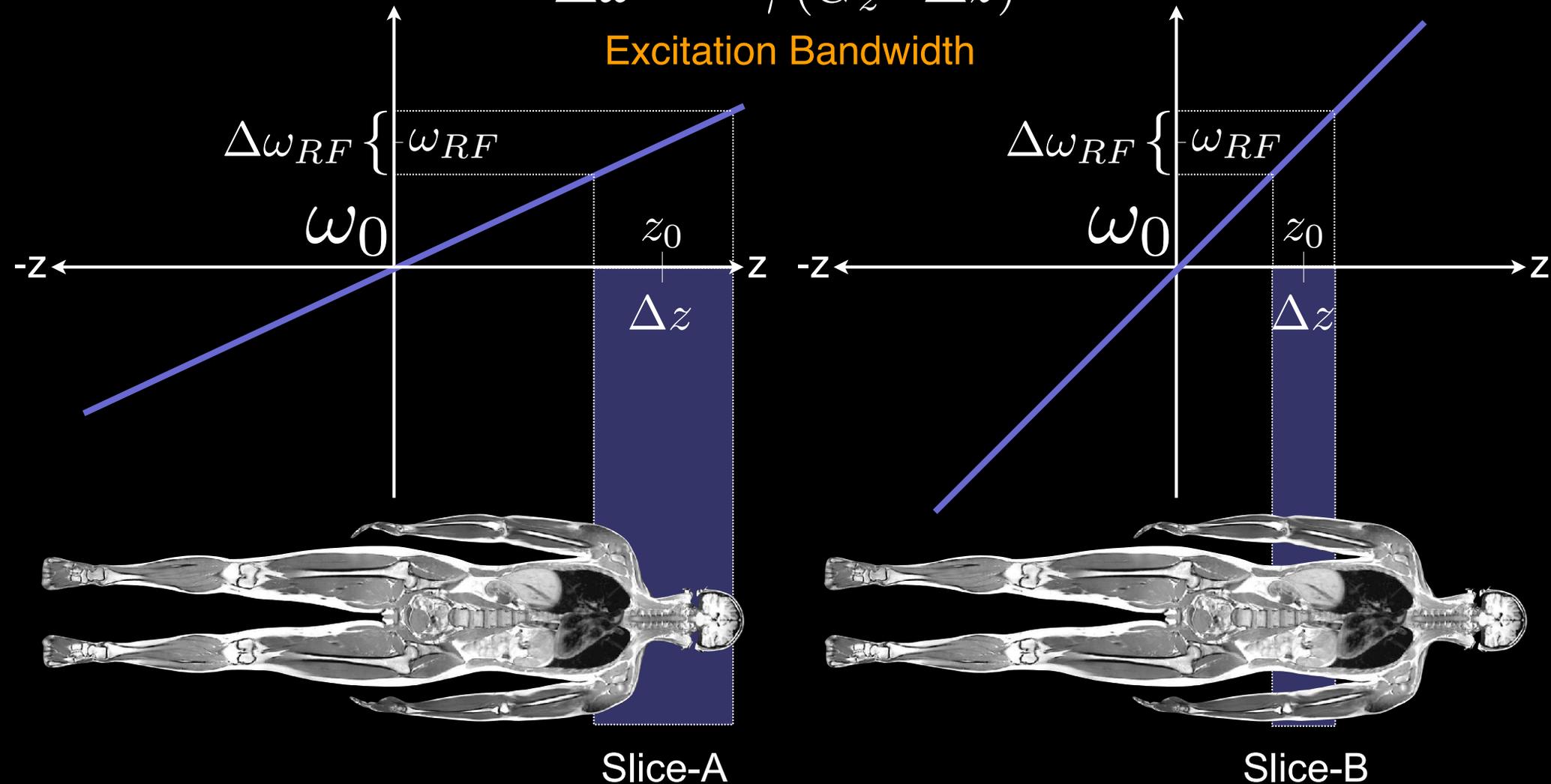
Slice-A

Slice-B

How do you move the slice along ±z?
Compare Δω and ω_RF for Slice-A and Slice-B.
Do we usually acquire ω_RF > ω_0?

Time Bandwidth Product (TBW)

- **Time bandwidth (TBW) product:**
  - **Pulse Duration [s] x Pulse Bandwidth [Hz]**
  - **Unitless**
  - **# of zero crossings**
  - **High TBW**
    - Large # of zero crossings ∴ fewer truncation artifacts
    - Longer duration pulse

- **Examples:**
  - **TBW = 4, RF = 1ms**
    - Excitation (RF) bandwidth?
    - Required G_z for 1cm slice?
  - **TBW = 16, RF = 1ms**
    - Excitation (RF) bandwidth?
    - Required G_z for 1cm slice?

Slice Selective Excitation - Example

$$\Delta\omega_{RF} = -\gamma\left(G_z \cdot \Delta z\right)$$ Excitation Bandwidth
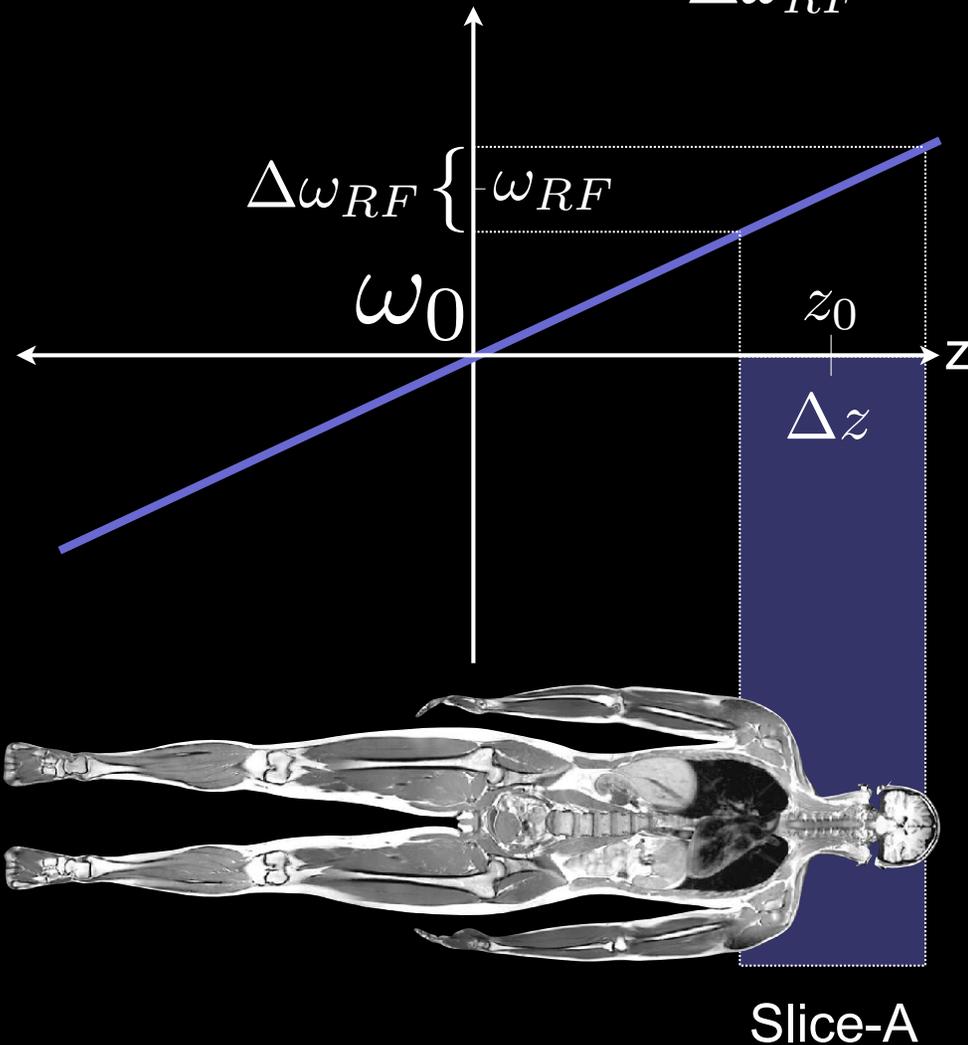
Slice-A

$$\mathrm{TBW} = \tau_{RF} \cdot \Delta\omega_{RF}$$

$$\Delta\omega_{RF} = \frac{\mathrm{TBW}}{\tau_{RF}}$$

$$= \frac{4}{1\mathrm{ms}}$$

$$= 4\mathrm{kHz}$$

$$G_z = \frac{\Delta\omega_{RF}}{\gamma\Delta z}$$

$$= \frac{4000\mathrm{Hz}}{42.57\mathrm{e}6\frac{\mathrm{Hz}}{\mathrm{T}}\frac{1\mathrm{T}}{10000\mathrm{G}} \cdot 10\mathrm{mm}}$$

$$= 0.94\frac{\mathrm{G}}{\mathrm{cm}}$$

Selective Excitation

- **What factors control slice selection?**

$$B_1^e \left(t \right)$$
Pulse envelope function
(e.g. $B_{1,max}$ and $\Delta\omega$)

$$\omega_{RF}$$
Excitation carrier frequency

BW
RF pulse bandwidth

$$\vec{G}$$
Gradient amplitude

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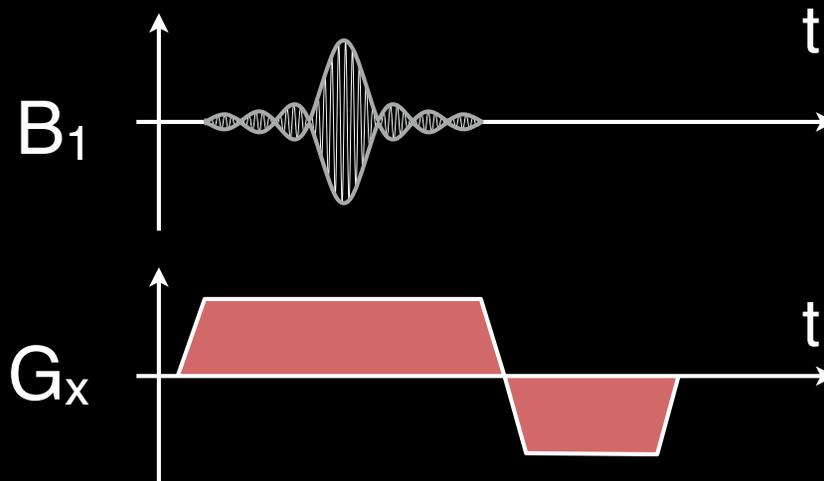
RF Pulse Bandwidth and Slice Profile:
Small Tip Angle Approximation

Bloch Equation (at on-resonance)

$$\frac{d\vec{M}_{rot}}{dt} = \vec{M}_{rot} \times \gamma \vec{B}_{eff}$$

where $\vec{B}_{eff} = \begin{pmatrix} B_1(t) \\ 0 \\ \cancel{B_0} - \frac{\omega}{\gamma} + G_z z \end{pmatrix}$

When we simplify the cross product,

$$\frac{d\vec{M}}{dt} = \begin{pmatrix} 0 & \omega(z) & 0 \\ -\omega(z) & 0 & \omega_1(t) \\ 0 & -\omega_1(t) & 0 \end{pmatrix} \vec{M}$$

$$\omega(z) = \gamma G_z z \qquad \omega_1(t) = \gamma B_1(t)$$

Small Tip Approximation

$$\frac{d\vec{M}}{dt} = \begin{pmatrix} 0 & \omega(z) & 0 \\ -\omega(z) & 0 & \omega_1(t) \\ 0 & -\omega_1(t) & 0 \end{pmatrix} \vec{M}$$

$M_z \approx M_0$ small tip-angle approximation

$\sin\theta \approx \theta$
$\cos\theta \approx 1$
$M_z \approx M_0 \rightarrow$ constant $\Bigg\}$ $\dfrac{dM_z}{dt} = 0$

$$\frac{dM_{xy}}{dt} = -i\gamma G_z z M_{xy} + i\gamma B_1(t) M_0$$

$$\boxed{M_{xy} = M_x + iM_y}$$

First order linear differential equation. Easily solved.

$$\frac{dM_{xy}}{dt} = -i\gamma G_z z M_{xy} + i\gamma B_1(t)M_0$$

Solving a first order linear differential equation:

$$M_{xy}(t,z) = i\gamma M_0 \int_0^t B_1(s)e^{-i\gamma G_z z \cdot (t-s)}ds$$
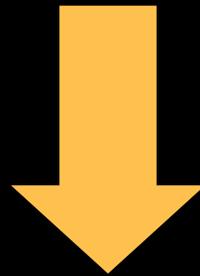
$$M_r(\tau,z) = iM_0 e^{-i\omega(z)\tau/2} \cdot \mathcal{FT}_{1D}\{\omega_1(t+\frac{\tau}{2})\}\,|_{f=-(\gamma/2\pi)G_z z}$$

(See the note for complete derivation)

$$M_r(\tau, z) = iM_0 e^{-i\omega(z)\tau/2} \cdot \mathcal{FT}_{1D}\{\omega_1(t + \frac{\tau}{2})\} \mid_{f=-(\gamma/2\pi)G_z z}$$

Small Tip Approximation

$$M_r(\tau, z) = iM_0 e^{-i\omega(z)\tau/2} \cdot \mathcal{FT}_{1D}\{\omega_1(t + \frac{\tau}{2})\} \, |_{f=-(\gamma/2\pi)G_z z}$$

Fourier transform

- For small tip angles, "the slice or frequency profile is well approximated by the Fourier transform of B1(t)"

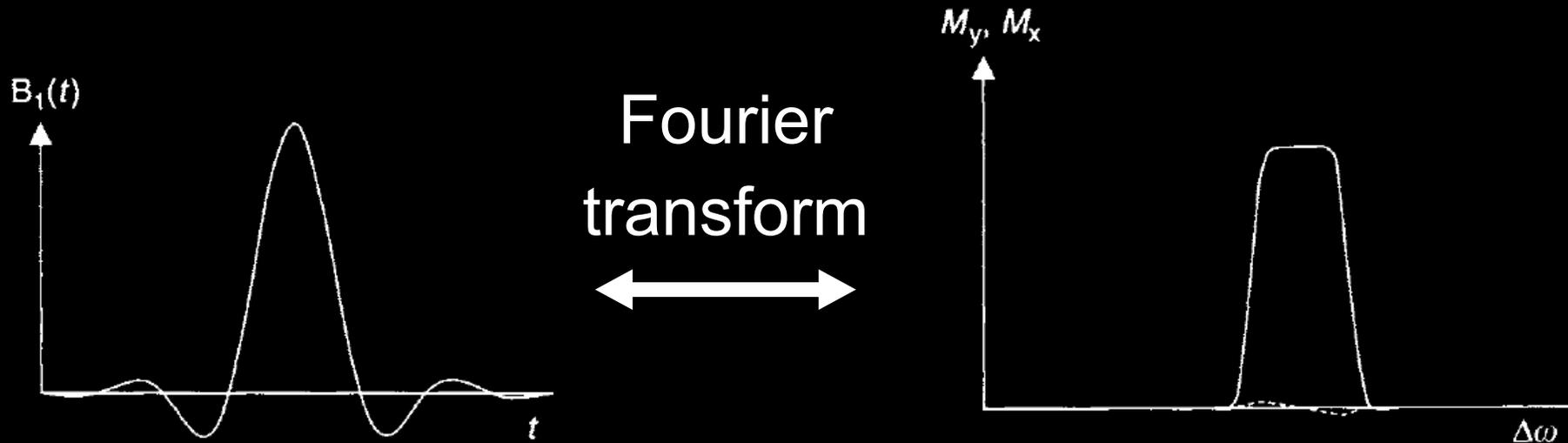- The approximation works surprisingly well even for flip angles up to 90°

Small Tip Approximation

the excitation profile, within the small angle approximation, is just the Fourier transform of the pulse

remember that the Bloch equations are non-linear and thus cannot be expected to behave linearly

the approximation works surprisingly well even for flip angles up to 90^0

Shaped Pulses
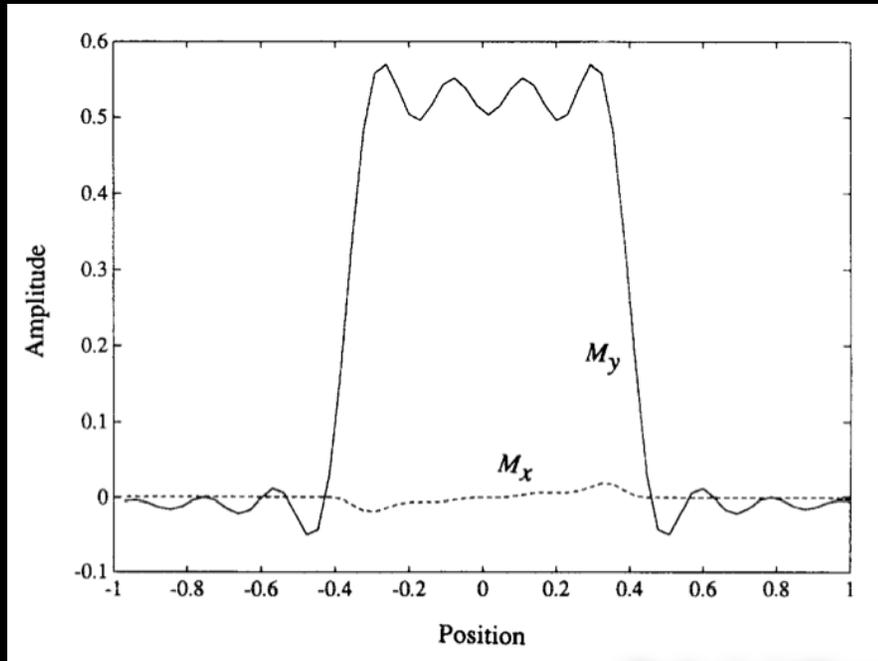
30°   90°
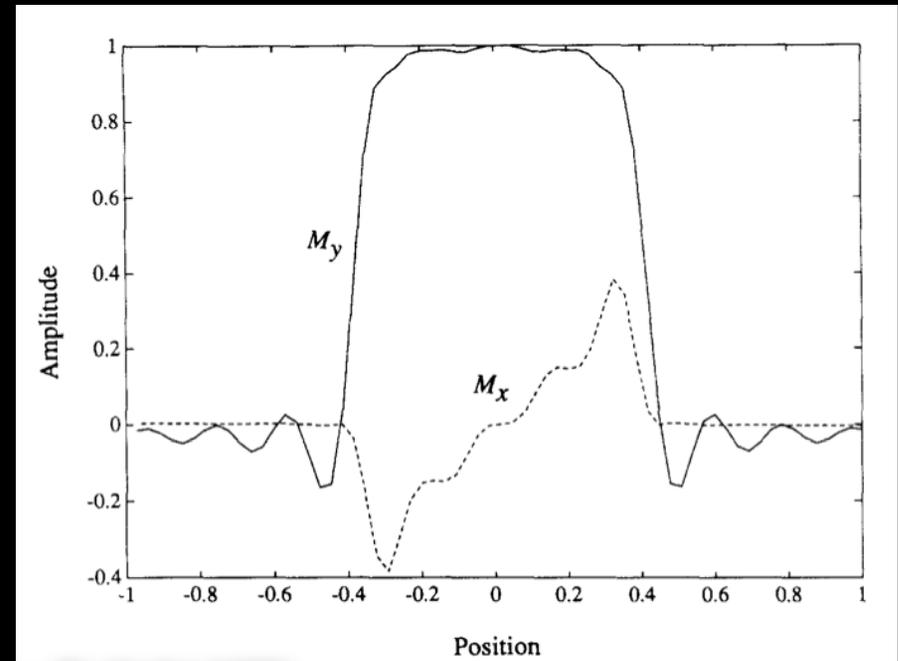
Pauly, J. *J. Magn. Reson.* **81** 43-56 (1989)

small-angle approximation still works reasonably
well for flip angles that aren't necessarily "small"

Truncation Artifacts

in MRI we want pulses to be as short as possible
to avoid relaxation effects

the sinc function is defined over all time
which is impractical in any experiment

the sinc pulse needs to be truncated to be
appropriate for clinical scans

Truncation Artifacts

what happens when we truncate our pulses?

non-uniform excitation

$\mathcal{FT}$

excited outside of slice
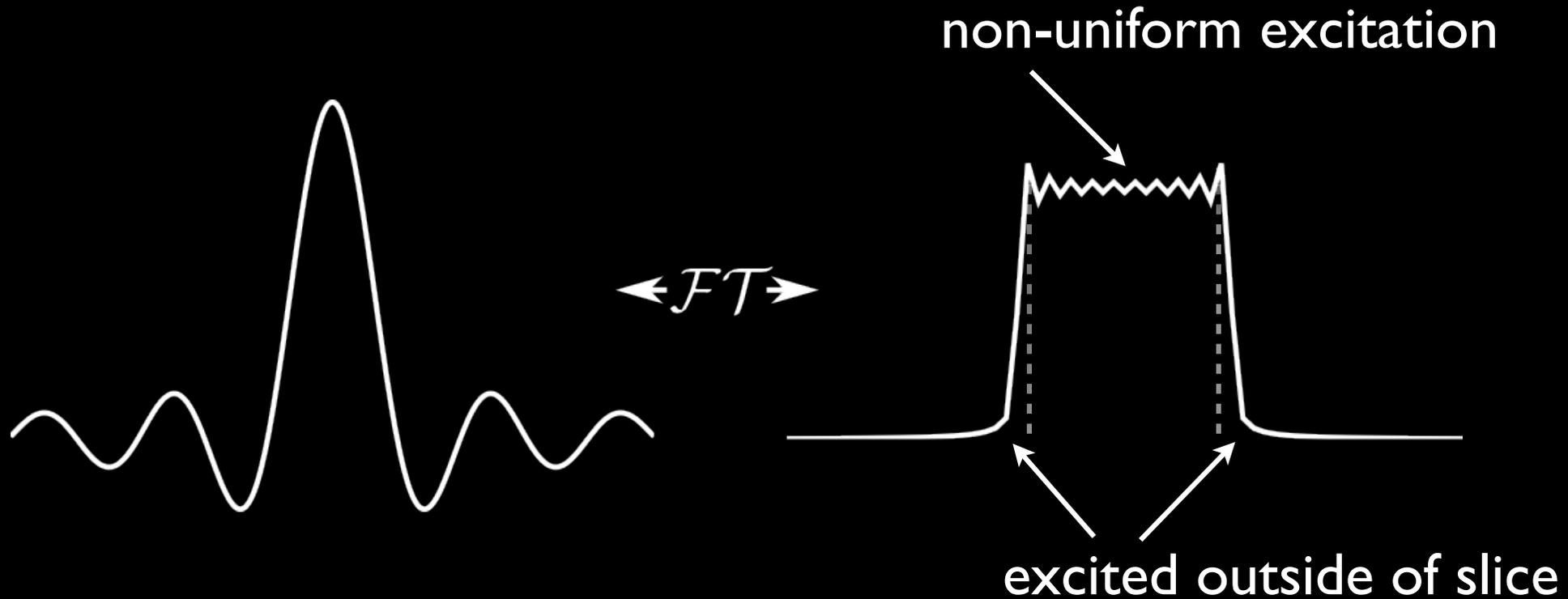
these deviations from the ideal are known
as truncation artifacts

Truncation Artifacts

alternative Pulse Shapes

gaussian

$$B_x(t) = A \exp\left[-a(t - \tau/2)^2\right]$$

reduced side-lobes, but not as flat of a profile

Window Functions

Hamming, Hanning, …

Slice Rewinder

RF

G_z

Spins rephased here

τ_p

$\tau_p/2$

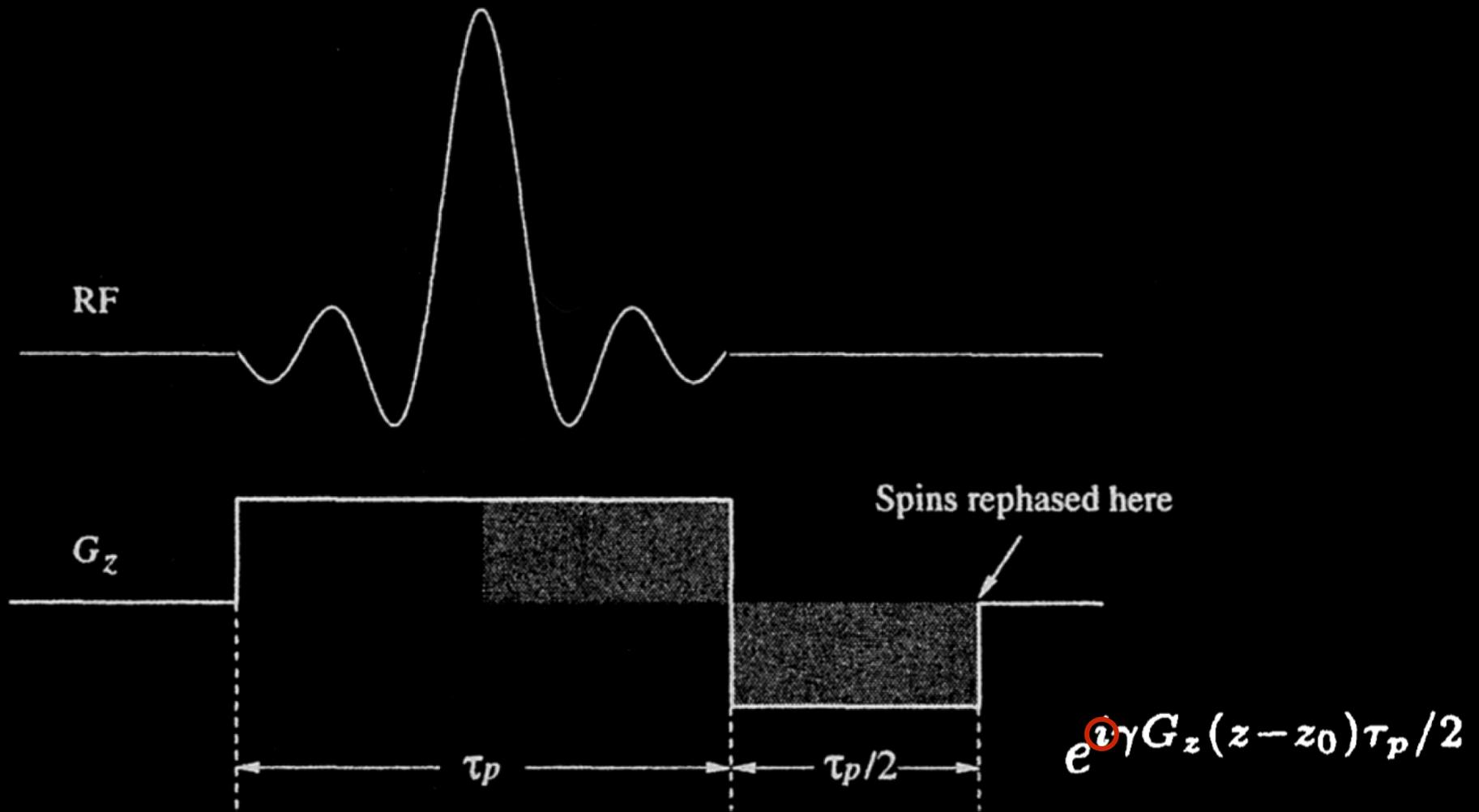$e^{i\gamma G_z (z - z_0) \tau_p / 2}$

Opposite Polarity

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Slice Selective Excitation Example
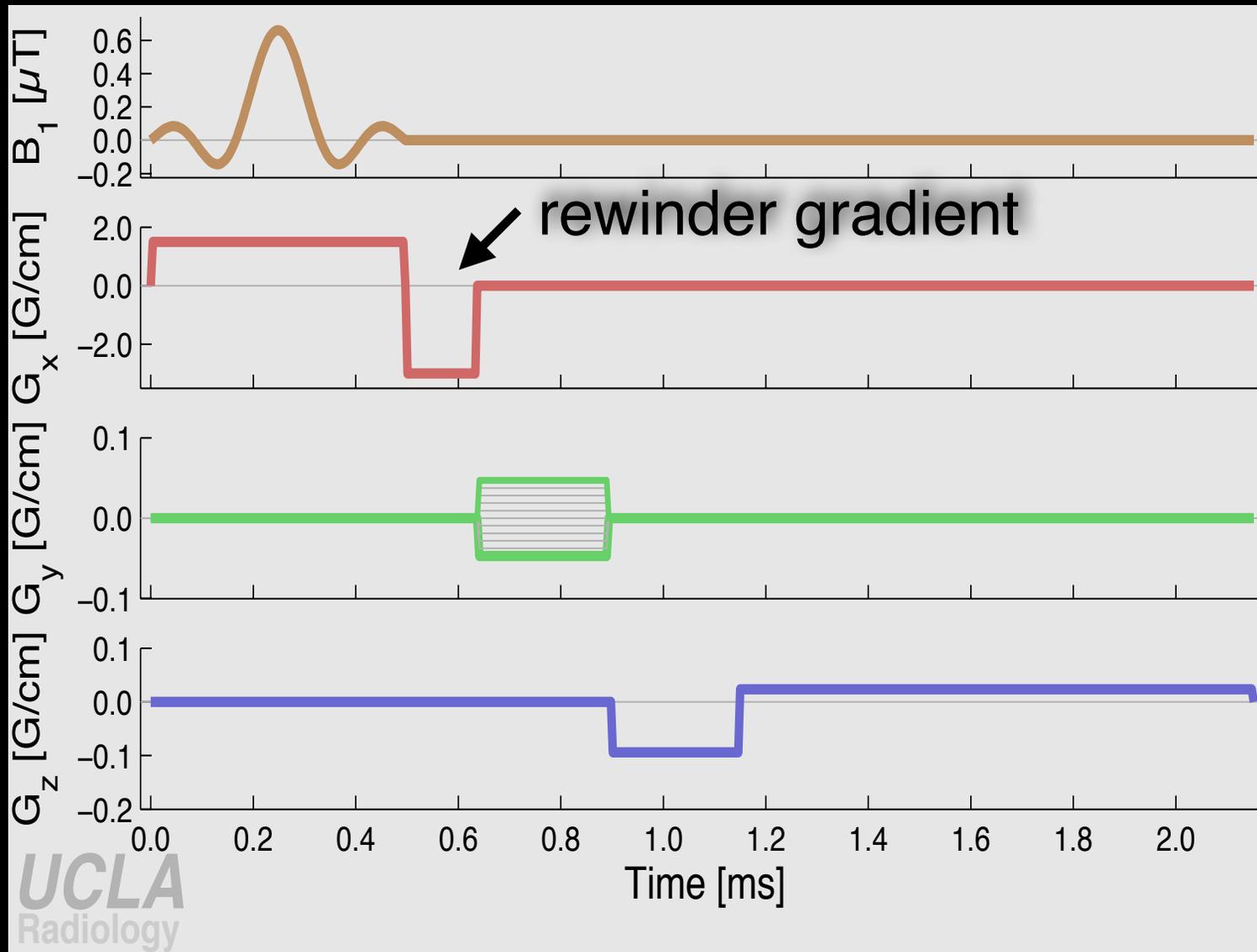
slice select gradient rewinder eliminates the linear phase ramp

Selective Excitation: Conclusion

B1 amplitude
-> flip angle

B1 amplitude profile
-> bandwidth, slice profile

B1 carrier frequency
-> slice location

B1 phase profile
-> slice location, etc.

Small Tip Approximation
-> slice profile = FT of B1 envelope function

MATLAB Demo

```matlab
%% Design of Windowed Sinc RF Pulses
tbw = 4;
samples = 512;
rf = wsinc(tbw, samples);
```

```matlab
%% Plot RF Amplitude
flip_angle = pi/2;
rf = flip_angle*rf;

pulseduration = 1;          % in msec
dt  = pulseduration/samples;
rfs = rf/(gamma*dt);        % Scaled to Gauss

bw = tbw/pulseduration; % in kHz
gmax = bw/gamma_2pi;

b1    = [rfs zeros(1,samples/2)];                          % in Gauss
g     = [ones(1,samples) -ones(1,samples/2)]*gmax;   % in G/cm
t_all = (1:length(g))*dt;   % in msec
```

MATLAB Demo

```matlab
%% Simulate Slice Profile using Bloch Simulation
x  = (-2:.01:2);                % in cm
f  = 0;                         % in Hz
dt = pulseduration/samples/1e3;
t  = (1:length(b1))*dt;   % in usec

% Bloch Simulation
[mx,my,mz] = bloch(b1(:),g(:),t(:),1,.2,f(:),x(:),0);

% Transverse Magnetization
mxy_bloch = mx+1i*my;
```

```matlab
%% Simulate Slice Profile using Small Tip Approximation
samples_st = 4096;
f_st = linspace(-0.5/dt,0.5/dt,samples_st)/1e3;
x_st = -f_st/(gamma_2pi*gmax);

rfs_zp = zeros(1,samples_st);
rfs_zp(1:samples) = rfs;

mxy_st = fftshift(fftn(fftshift(rfs_zp)))/30;
```

Questions?

- Related reading materials
    - Nishimura - Chap 6.1, 6.2, 6.4

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